



CDS 101/110: Lecture 3.3

Some Details on Linear Systems

Goals for Today:

- Review Convolution Integral (again!): board notes
- Sampled Data Systems
- Cart-Pendulum problem

Reading:

- Åström and Murray, FBS-2e, Ch. 6.4 (assuming you read 6.1-6.3)



Linear Discrete Time Control Systems

Basic Form of Linear Discrete-Time control system. $t_{k+1} - t_k = dt$

$$\begin{aligned}
 & - x(t = t_{k+1}) = A_k x(t = t_k) + B_k u(t = t_k); \\
 & \quad y(t = t_k) = C_k x(t = t_k) + D_k u(t = t_k) \\
 & - \quad x_{k+1} = A_k x_k + B_k u_k; \quad y_k = C_k x_k + D_k u_k \\
 & - \quad x[k + 1] = Ax[k] + Bu[k]; \quad y[k] = Cx[k] + Du[k]
 \end{aligned}$$

} General Form
 } Some Common Notation

Sampled Data System (using Convolution Integral)

- $x(t + dt) = e^{A dt} x(t) + \int_t^{t+dt} e^{A(t+dt-\tau)} B u(\tau) d\tau = \Phi x(t) + \Gamma u(t)$

- $\Phi = e^{A dt}$

- $\Gamma = \left(\int_0^{dt} e^{As} ds \right) B = A^{-1} (e^{A dt} - I) B$

LTI

Must make Assumption about $u(\tau)$

Assumes zero-order hold

If A invertible



Linear Discrete Time Control Systems

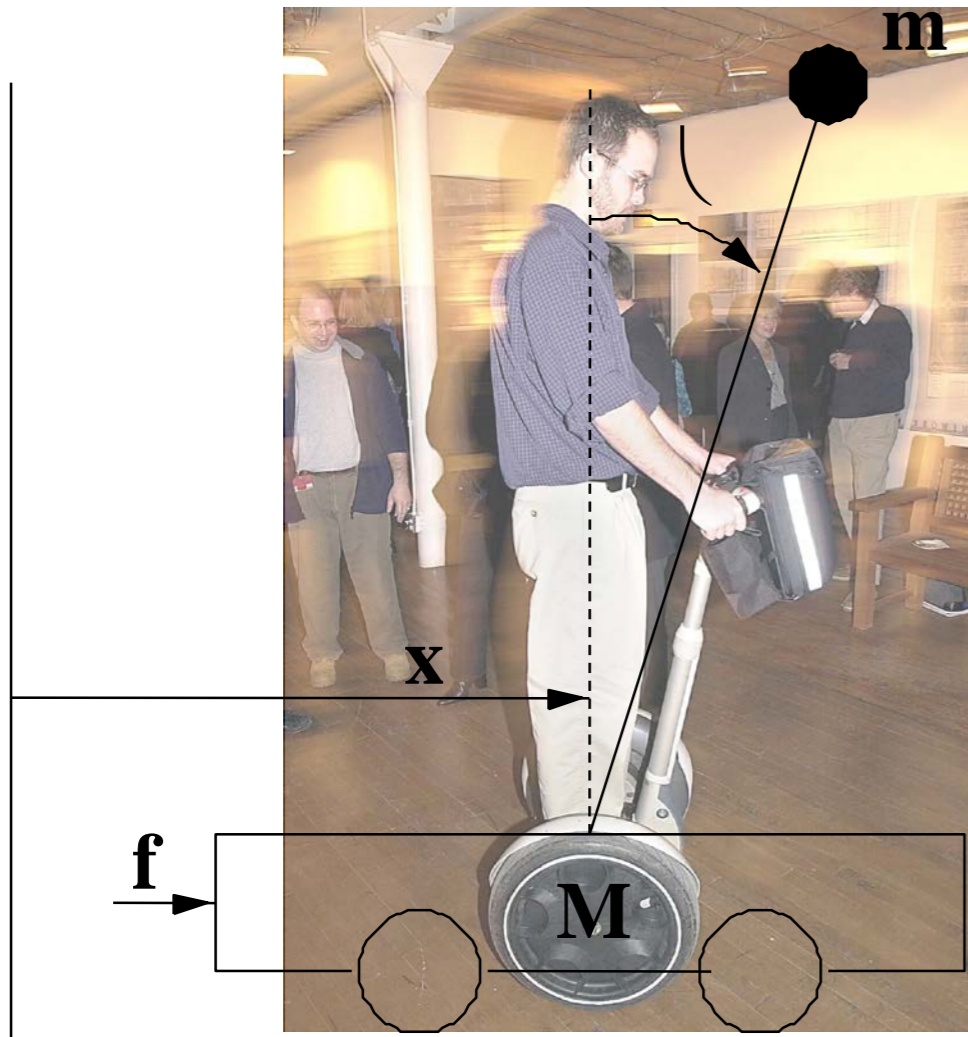
Inverse between sampled/continuous time representations (LTI)

$$- A = \frac{1}{dt} \log(\Phi) ; \quad B = \left(\int_0^{dt} e^{As} ds \right)^{-1} \Gamma$$

Stability: $x_{k+1} = Ax_k$

- $x_1 = Ax_0; \quad x_2 = Ax_1 = A^2x_0; \quad \dots ; \quad x_n = A^n x_0$
- $\lim_{n \rightarrow \infty} A^n x_0 = 0$ if $\rho(A) < 1$, where
$$\rho(A) = \max\{|\lambda| : \lambda \text{ is an eigenvalue of } A\}$$

Example: Inverted Pendulum on a Cart



$$(M + m)\ddot{x} + ml \cos \theta \ddot{\theta} = -b\dot{x} + ml \sin \theta \dot{\theta}^2 + f$$

$$(J + ml^2)\ddot{\theta} + ml \cos \theta \ddot{x} = -mgl \sin \theta$$

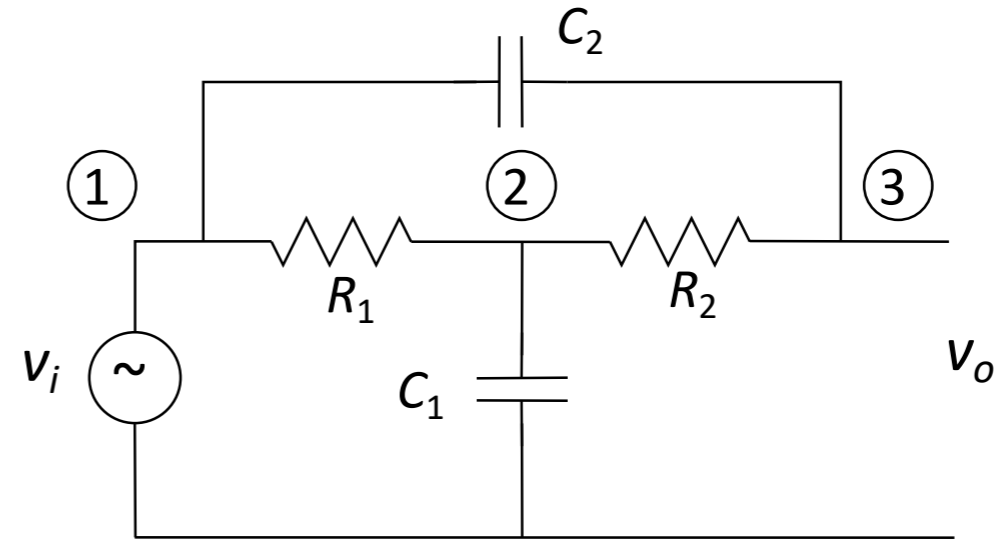
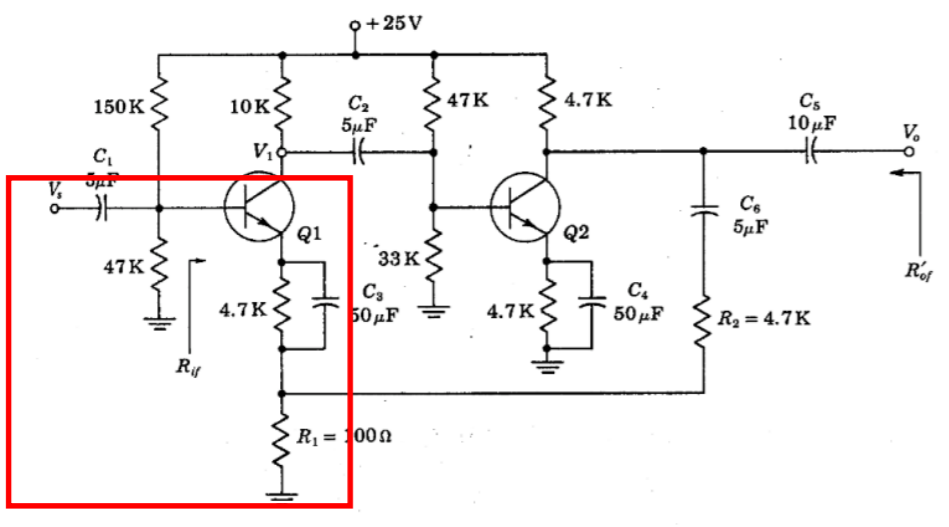
- State: $x, \theta, \dot{x}, \dot{\theta}$
- Input: $u = F$
- Output: $y = x$
- Linearize according to previous formula around $\theta = 0$

$$\frac{d}{dt} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & \frac{m^2 g l^2}{J(M + m) + M m l^2} & \frac{-(J + m l^2) b}{J(M + m) + M m l^2} & 0 \\ 0 & \frac{m g l (M + m)}{J(M + m) + M m l^2} & \frac{-m l b}{J(M + m) + M m l^2} & 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \\ \frac{J + m l^2}{J(M + m) + M m l^2} \\ \frac{m l}{J(M + m) + M m l^2} \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \\ \dot{x} \\ \dot{\theta} \end{bmatrix}$$



Example: Electrical Circuit



“Bridged Tee Circuit”

- Derivation based on Kirchoff’s laws for electrical circuits (Ph 2)

- Sum of currents at nodes = 0:

$$C_1 \frac{dv_2}{dt} = \frac{v_1 - v_2}{R_1} - \frac{v_2 - v_3}{R_2}$$

$$C_2 \frac{d(v_3 - v_1)}{dt} = -\frac{v_3 - v_2}{R_2}$$

- Rewrite in terms of new states: $v_{c1} = v_2$, $v_{c2} = v_3 - v_1$

$$\frac{d}{dt} \begin{bmatrix} v_{c1} \\ v_{c2} \end{bmatrix} = \begin{bmatrix} -\frac{1}{C_1} \left(\frac{1}{R_1} + \frac{1}{R_2} \right) & -\frac{1}{C_1 R_2} \\ -\frac{1}{C_2 R_2} & -\frac{1}{C_2 R_2} \end{bmatrix} \begin{bmatrix} v_{c1} \\ v_{c2} \end{bmatrix} + \begin{bmatrix} \frac{1}{C_1} \left(\frac{1}{R_1} + \frac{1}{R_2} \right) \\ \frac{1}{C_2 R_2} \end{bmatrix} v_i \quad \left| \quad v_o = \begin{bmatrix} 0 & -1 \end{bmatrix} \begin{bmatrix} v_{c1} \\ v_{c2} \end{bmatrix} + v_i$$