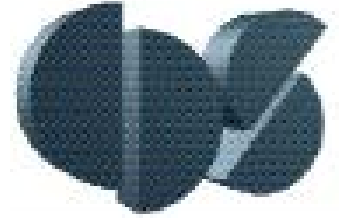




CDS 101/110: Lecture 6.2

Transfer Functions



November 2, 2016

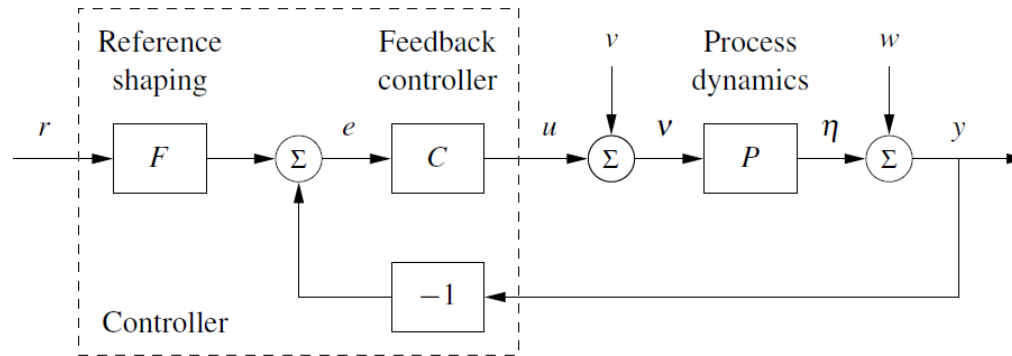
Goals:

- Continued study of Transfer functions
- Review Laplace Transform
- “Block Diagram Algebra”
- Bode Plot Intro

Reading:

- Åström and Murray, Feedback Systems-2e, Chapter 9

Transfer Functions



Exponential response of a linear state space system

$$y(t) = \underbrace{C e^{At} (x(0) - (sI - A)^{-1} B)}_{\text{transient}} + \underbrace{(C(sI - A)^{-1} B + D) e^{st}}_{\text{steady state}}$$

Transfer function

- Steady state response is proportional to exponential input => look at input/output ratio $y(s)/u(s)$
- $G(s) = C(sI - A)^{-1} B + D$ is the transfer function between input and output

2

Frequency response (system response to pure sinusoidal input)

$$u(t) = M \sin \omega t = \frac{M}{2i} (e^{i\omega t} - e^{-i\omega t})$$

$$y_{ss}(t) = \frac{M}{2i} (G(i\omega) e^{i\omega t} - G(-i\omega) e^{-i\omega t}) = M |G(i\omega)| \sin(\omega t + \arg G(i\omega))$$

gain
phase

Laplace Transform Review

Definition: given a “suitable” function $y(t)$ the Laplace Transform of y is:

$$\mathcal{L}\{y(t)\} = \int_0^{\infty} y(\tau)e^{-s\tau} d\tau$$

Defined on entire complex plane

Properties:

- **Linearity:** $\mathcal{L}\{\alpha f(t) + \beta g(t)\} = \alpha \mathcal{L}\{f(t)\} + \beta \mathcal{L}\{g(t)\}$, for $\alpha, \beta \in \mathbb{R}$
- **Derivative:** $\mathcal{L}\left\{\frac{d}{dt}x(t)\right\} = s\mathcal{L}\{x(t)\} - x(0)$
 - More generally, $\mathcal{L}\left\{\frac{d^n}{dt^n}x(t)\right\} = s^n \mathcal{L}\{x(t)\} - \sum_{k=1}^n s^{k-1} x^{n-k}(0)$

• **Proof:**

$$\int_0^{\infty} \frac{d}{dt}(x(t)e^{-st}) dt = x(t)e^{-st} \Big|_0^{\infty} = \int_0^{\infty} \frac{dx}{dt} e^{-st} dt - s \int_0^{\infty} x(t)e^{-st} dt$$

$$-x(0) = \mathcal{L}\left\{\frac{dx}{dt}\right\} - s\mathcal{L}\{x(t)\}$$

Laplace Transform Review

- **Integral:** $\mathcal{L}\left\{\int_0^t x(t) dt\right\} = \frac{1}{s}\mathcal{L}\{x(t)\}$
- **Convolution:** $\mathcal{L}\{h(t) * g(t)\} = H(s)G(s)$

Proof: $\mathcal{L}\{h(t) * g(t)\} = \int_0^\infty (h(t) * g(t))e^{-st} dt$

If $h(t)$ is *causal* ($h(t) = 0$ for $t < 0$), then $h(t) * g(t) = \int_0^t h(t - \tau)g(\tau)d\tau$

$$\begin{aligned}\mathcal{L}\{h(t) * g(t)\} &= \int_0^\infty \int_0^t h(t - \tau) g(\tau) e^{-st} d\tau dt = \int_0^\infty \int_\tau^\infty h(t - \tau) g(\tau) e^{-st} dt d\tau \\ &= \int_0^\infty \int_0^\infty h(\mu) g(\tau) e^{-s(\mu+\tau)} d\mu d\tau = \int_0^\infty h(\mu) e^{-s\mu} d\mu \int_0^\infty g(\tau) e^{-s\tau} d\tau = H(s)G(s)\end{aligned}$$

- **Exponential:**

- $\mathcal{L}\{e^{-at}\} = \int_0^\infty e^{-(s+a)t} dt = \frac{-1}{s+a} e^{-(s+a)t} \Big|_0^\infty = \frac{1}{s+a}$

- $\mathcal{L}\{e^{-At}\} = (sI - A)^{-1} = \frac{\text{adj}(sI - A)}{\det(sI - A)}$

Laplace Transform Review

- **Transfer Function:**

$$\dot{x} = Ax + Bu \quad \Rightarrow_{\mathcal{L}} \quad sX(s) - x(0) = AX(s) + BU(s)$$

$$y = Cx + Du \quad \Rightarrow_{\mathcal{L}} \quad Y(s) = CX(s) + DU(s)$$

$$X(s) = (sI - A)^{-1}B U(s) + (sI - A)^{-1}x(0)$$

$$Y(s) = (C(sI - A)^{-1}B + D)U(s) + C(sI - A)^{-1}x(0)$$

When $x(0) = 0$, $\Rightarrow \quad \frac{Y(s)}{U(s)} = G(s) = C(sI - A)^{-1}B + D$

- **Impulse Response:** $y(t) = \int_0^{\infty} h(t - \tau)u(\tau)d\tau$

$$Y(s) = \mathcal{L}\{y(t)\} = \int_0^{\infty} e^{-st} y(t)dt = \int_0^{\infty} e^{-st} \int_{0\infty}^{\infty} h(t - \tau)u(\tau)d\tau dt$$

$$= \int_0^{\infty} \int_0^t e^{-s(t-\tau)} e^{-s\tau} h(t - \tau)u(\tau)d\tau dt = \int_0^{\infty} e^{-s\tau} u(\tau)d\tau \int_0^{\infty} e^{-st} h(t)dt$$

$$= H(s)U(s)$$

Therefore, $G(s) = \mathcal{L}\{h(t)\}$ =Laplace Transform of system Impulse Response

Laplace Transform Review

Constant Coefficient O.D.E.: Laplace Transform (assuming zero initial conditions)

$$\mathcal{L}\{\cdot\} \begin{cases} \frac{d^n}{dt^n} y(t) + a_1 \frac{d^{n-1}}{dt^{n-1}} y(t) + \dots + a_n y(t) = b_1 \frac{d^{n-1}}{dt^{n-1}} u(t) + \dots + b_n u(t) \quad (*) \\ (s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n) Y(s) = (b_1 s^{n-1} + \dots + b_n) U(s) \\ G(s) = \frac{Y(s)}{U(s)} = \frac{(b_1 s^{n-1} + \dots + b_n)}{(s^n + a_1 s^{n-1} + \dots + a_{n-1} s + a_n)} = \frac{n(s)}{d(s)} \end{cases}$$

- Roots of $d(s)$ are called the *poles* of transfer function $G(s)$
 - If p is a system pole, then $y = e^{pt}$ is a solution to (*) with $u(t) = 0$
 - Poles are strictly defined by matrix A .
- Roots of $n(s)$ are called the *zeros* of $G(s)$
 - If s is a pole of $G(s)$, then $G(s)e^{st}$ is an output if $d(s) \neq 0$.
 - Out put is zero at s if $n(s) = 0$.

Poles and Zeros

$$\dot{x} = Ax + Bu$$
$$y = Cx + Du$$

$$G(s) = \frac{n(s)}{d(s)}$$
$$d(s) = \det(sI - A)$$

- Roots of $d(s)$ are called *poles* of $G(s)$
- Roots of $n(s)$ are called *zeros* of $G(s)$

Poles of $G(s)$ determine the stability of the (closed loop) system

- Denominator of transfer function = characteristic polynomial of state space system
- Provides easy method for computing stability of systems
- Right half plane (RHP) poles ($\text{Re} > 0$) correspond to unstable systems

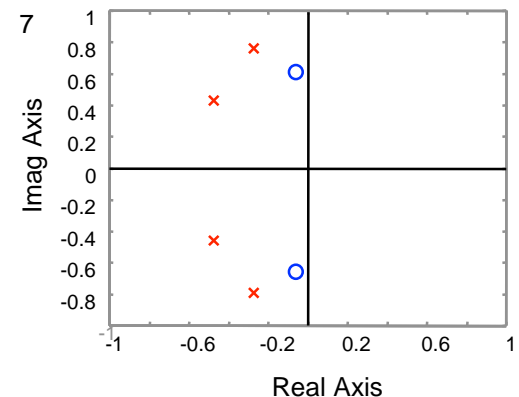
Zeros of $G(s)$ related to frequency ranges with limited transmission

- A pure imaginary zero at $s = i\omega$ blocks any output at that frequency ($G(i\omega) = 0$)
- Zeros provide limits on performance, especially RHP zeros

MATLAB: `pole(G)`, `zero(G)`, `pzmap(G)`

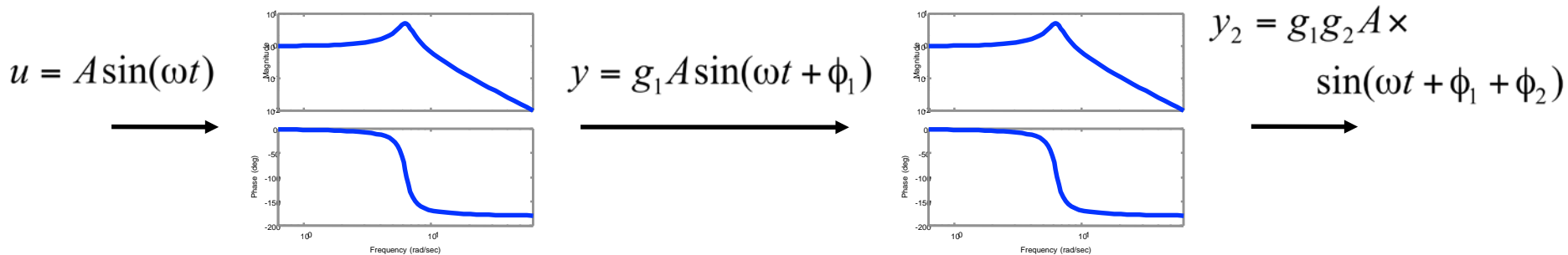
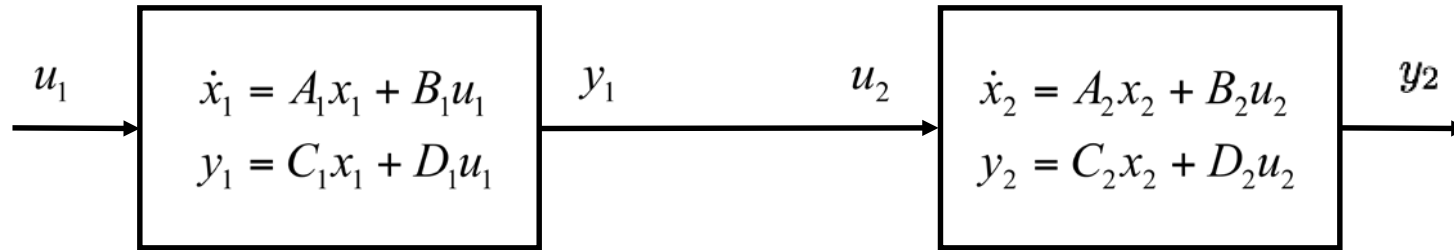
$$G(s) = k \frac{s^2 + b_1s + b_2}{s^4 + a_1s^3 + a_2s^2 + a_3s + a_4}$$

`pzmap(G)`



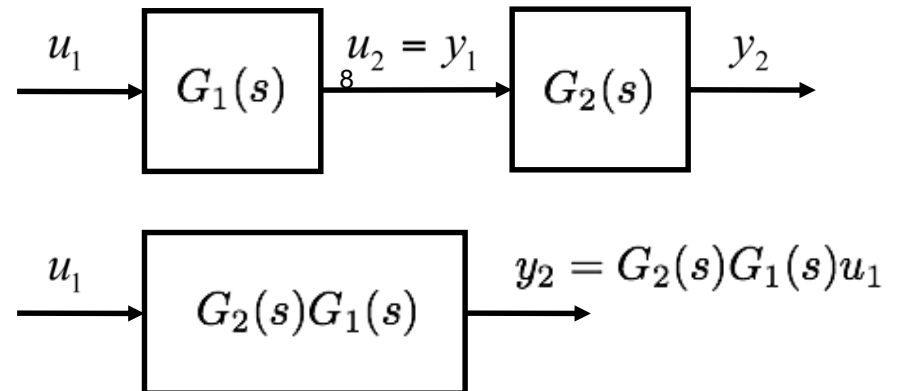
Series Interconnections

Q: what happens when we connect two systems together in series?

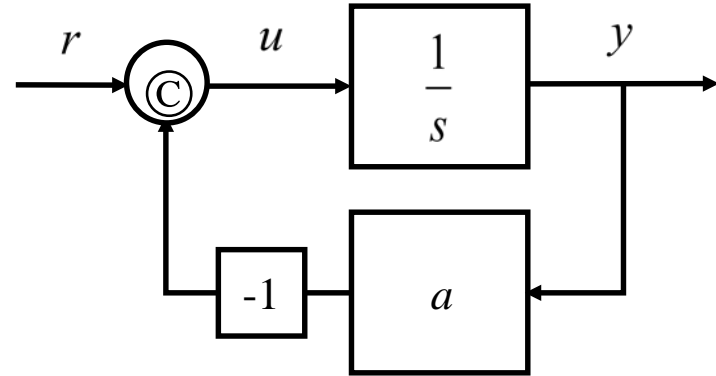
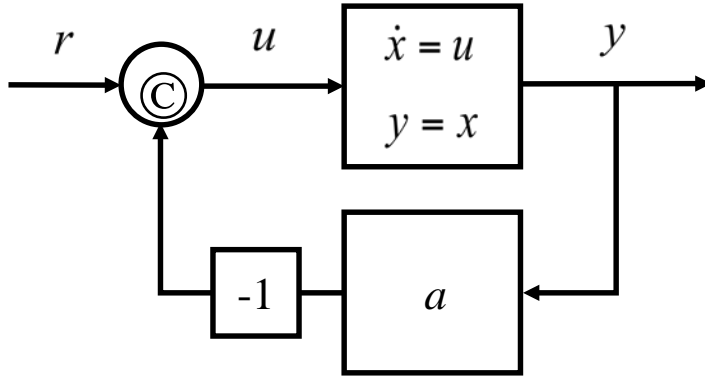


A: Transfer functions multiply

- Gains multiply, phases add
- Generally: transfer functions well formulated for frequency domain interconnections
 - Convolution \rightarrow multiplication
- MATLAB/python: `G = series(G1, G2)`



Feedback Interconnection



State space derivation

$$\dot{x} = u = r - ay = -ax + r$$

$$y = x$$

Frequency response $r = A \sin(\omega t)$

$$y = \left| \frac{1}{\sqrt{a^2 + \omega^2}} \right| \sin \left(\omega t - \tan^{-1} \left(\frac{\omega}{a} \right) \right)$$

Transfer function derivation

$$y = \frac{u}{s} = \frac{r - ay}{s}$$

$$y = \frac{r}{s + a} = G(s)r$$

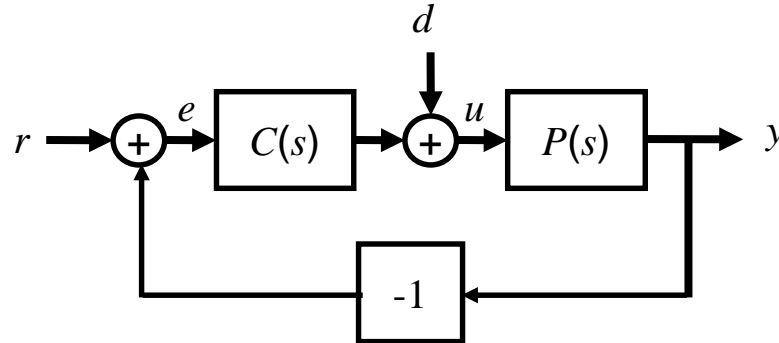
Frequency response

$$y = |G(i\omega)| \sin(\omega t + \angle G(i\omega))$$

- MATLAB: `G = feedback(sys, a)` ← works for either state space or transfer functions

Block Diagram Algebra

Basic idea: treat transfer functions as multiplication, write down equations



$$y = P(s)u$$

$$u = d + C(s)e$$

$$e = r - y$$

Manipulate equations to compute desired signals

$$e = r - y$$

$$= r - P(s)u$$

$$= r - P(s)(d + C(s)e)$$

$$(1 + P(s)C(s))e = r - P(s)d$$

$$e = \underbrace{\frac{1}{1 + P(s)C(s)}}_{H_{er}} r - \underbrace{\frac{P(s)}{1 + P(s)C(s)}}_{H_{ed}} d$$

Note: linearity gives superposition of terms

Algebra works because we are working in frequency domain

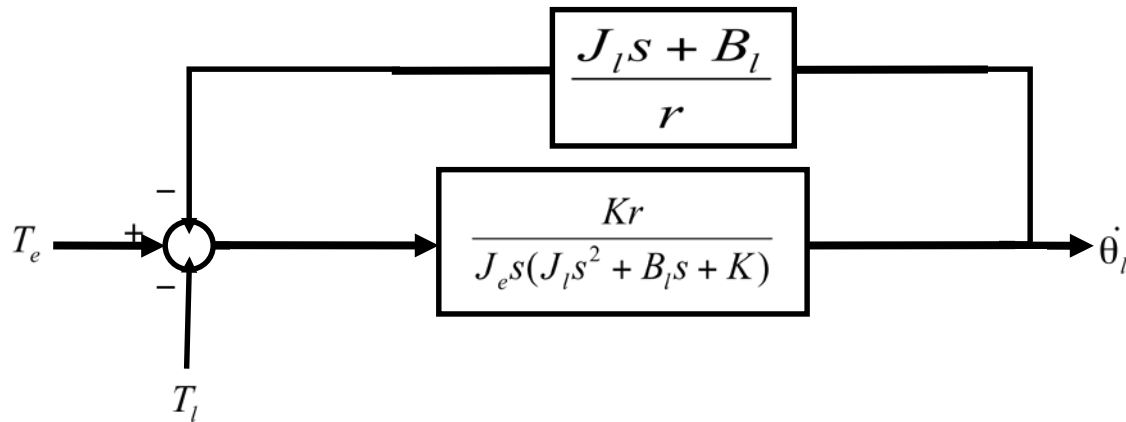
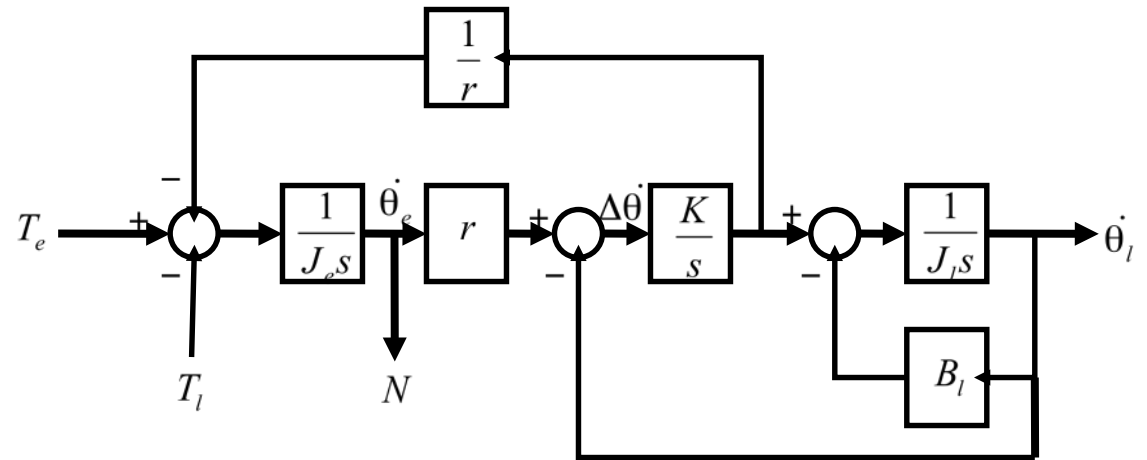
- Time domain (ODE) representations are not as easy to work with
- Formally, all of this works because of Laplace transforms

Block Diagram Algebra

Type	Diagram	Transfer function
Series		$H_{y_2u_1} = H_{y_2u_2} H_{y_1u_1} = \frac{n_1 n_2}{d_1 d_2}$
Parallel		$H_{y_3u_1} = H_{y_2u_1} + H_{y_1u_1} = \frac{n_1 d_2 + n_2 d_1}{d_1 d_2}$
Feedback		$H_{y_1r} = \frac{H_{y_1u_1}}{1 + H_{y_1u_1} H_{y_2u_2}} = \frac{n_1 d_2}{n_1 n_2 + d_1 d_2}$

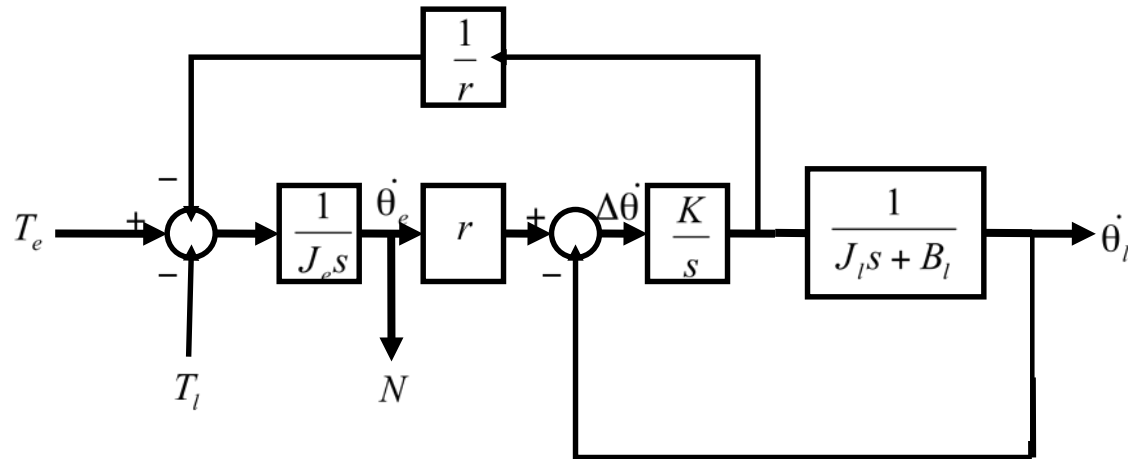
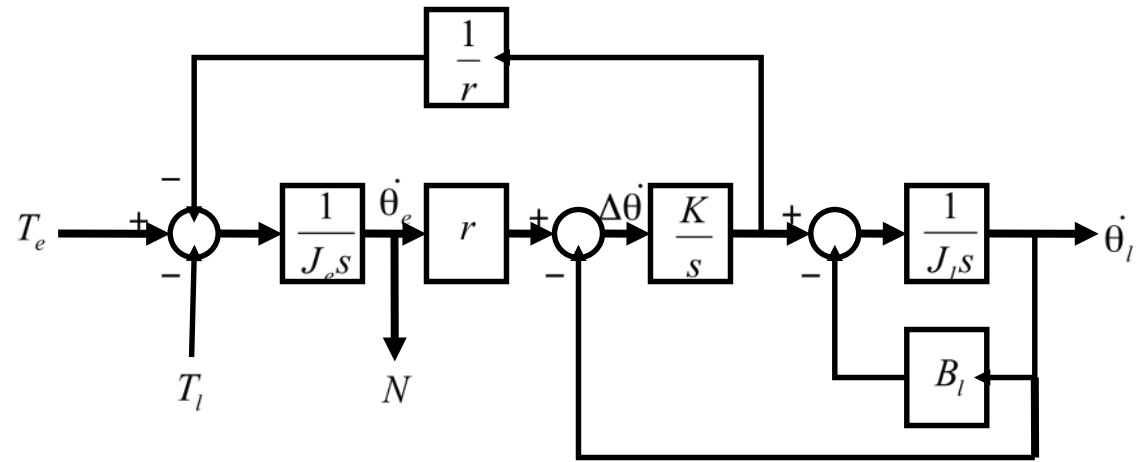
- These are the basic manipulations needed; some others are possible
- Formally, could work all of this out using the original ODEs (\Rightarrow nothing really new)

Example: Engine Control of a GM Astro

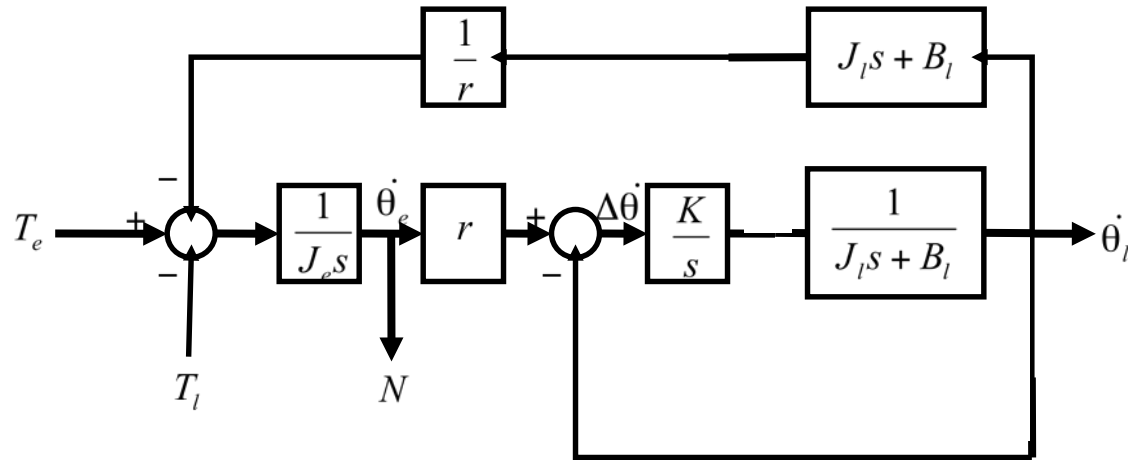
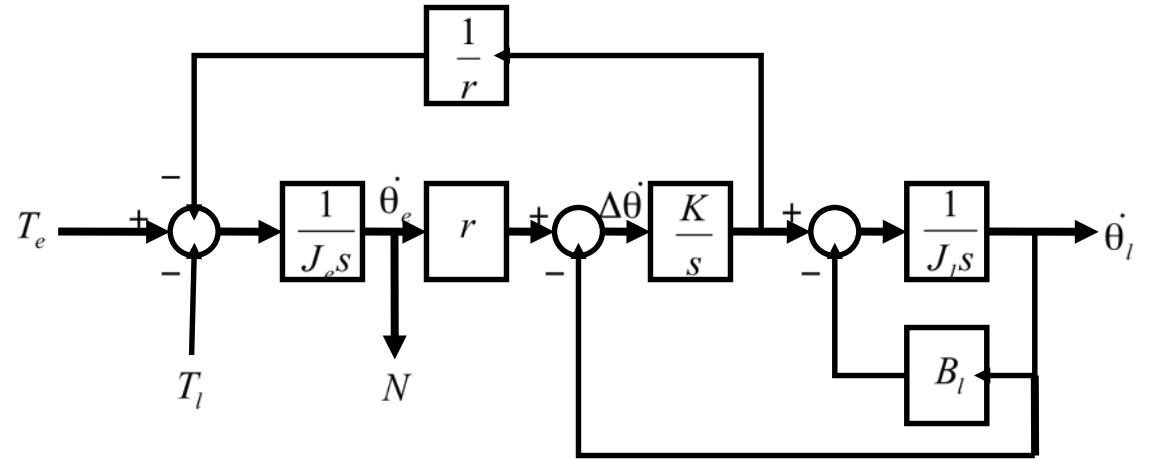


$$H_{\theta_l T_e}(s) = \frac{Kr}{J_e J_l s^3 + J_e B_l s^2 + (J_e K + K J_l) s + K B_l}$$

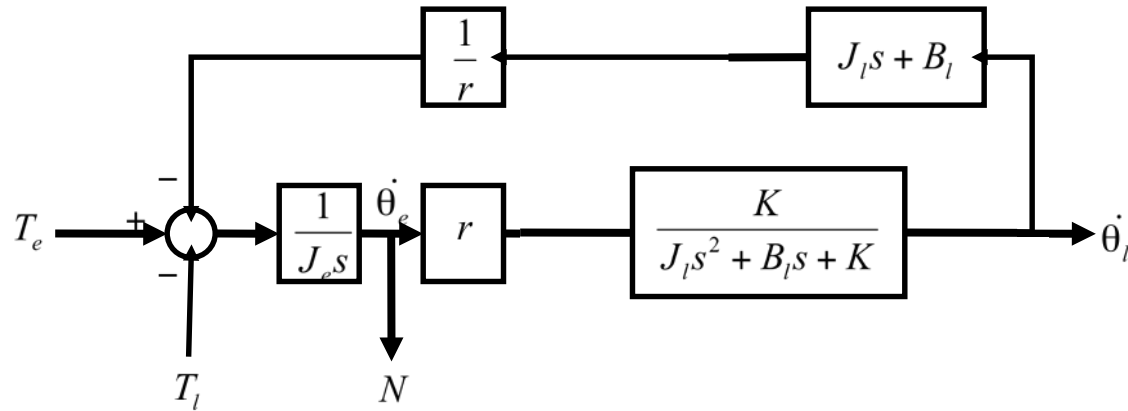
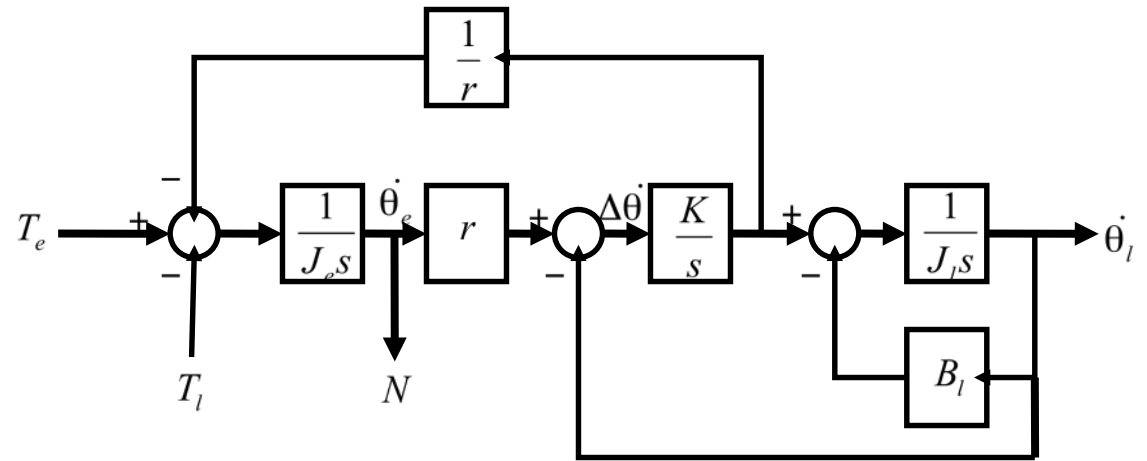
Example: Engine Control of a GM Astro



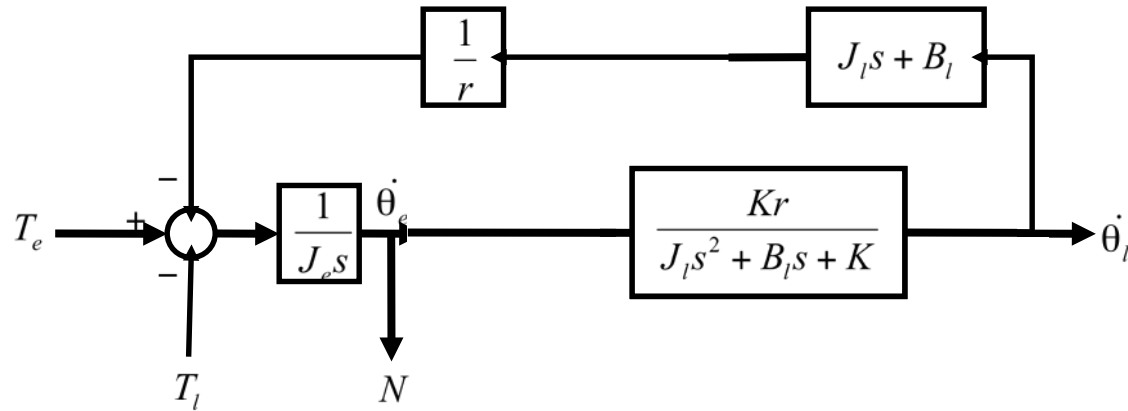
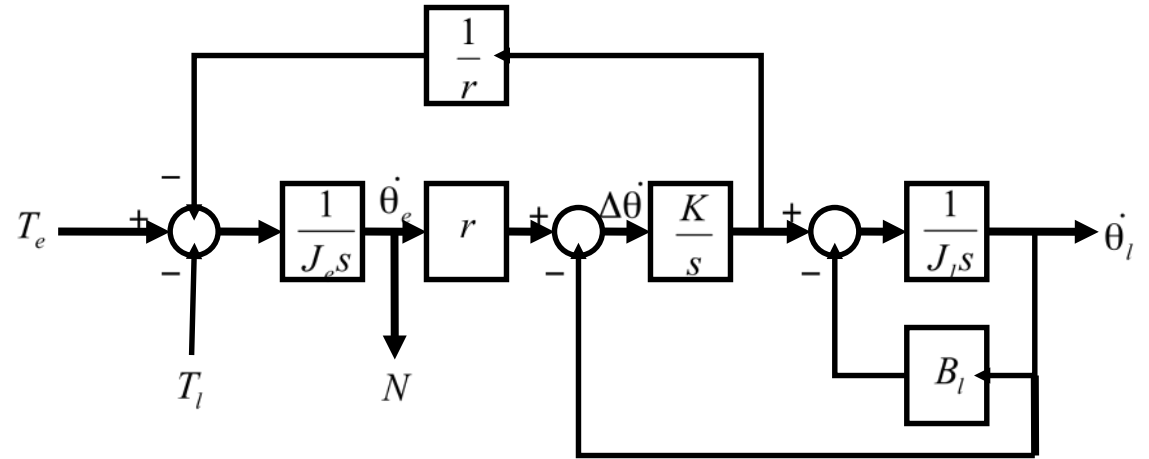
Example: Engine Control of a GM Astro



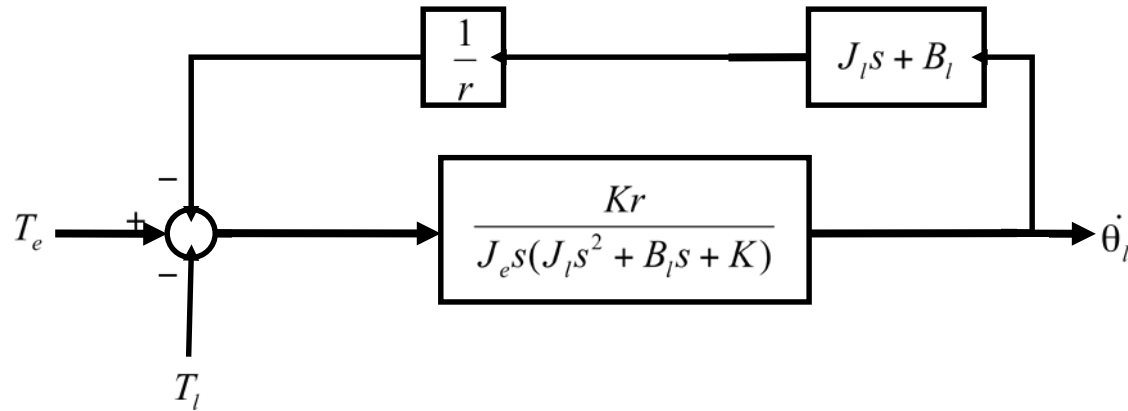
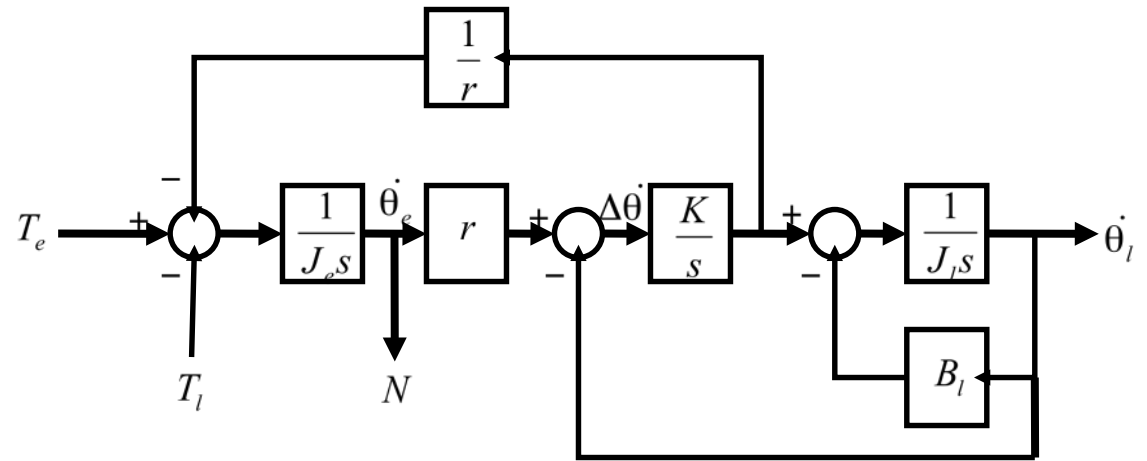
Example: Engine Control of a GM Astro



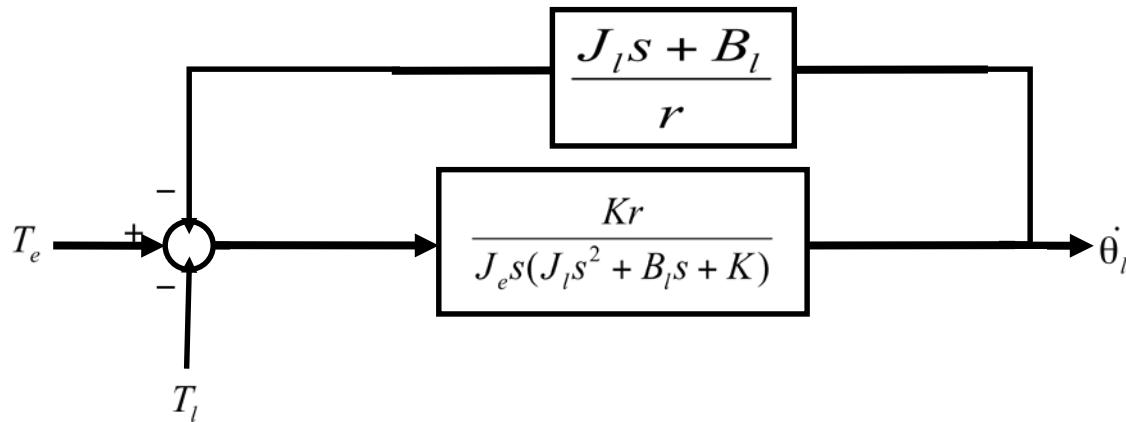
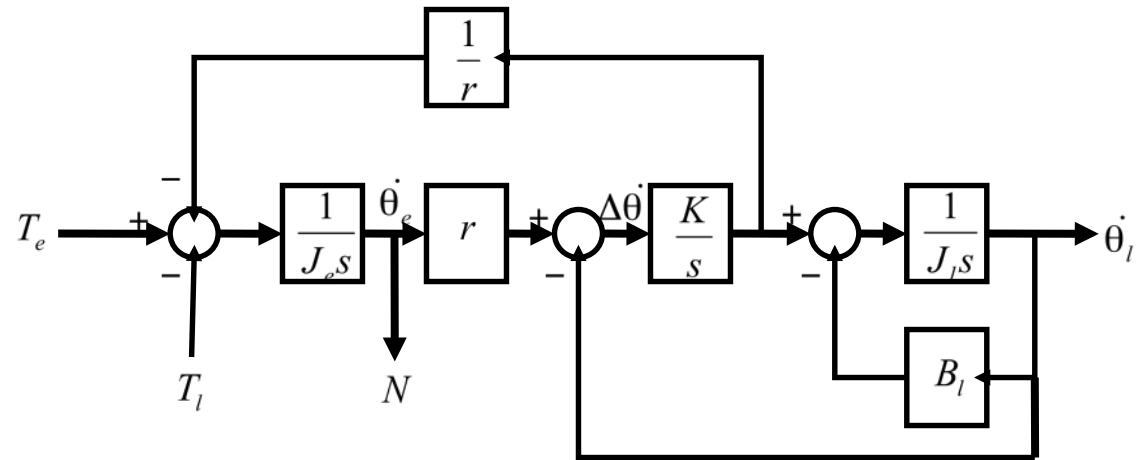
Example: Engine Control of a GM Astro



Example: Engine Control of a GM Astro



Example: Engine Control of a GM Astro



$$H_{\theta_l T_e}(s) = \frac{Kr}{J_e J_l s^3 + J_e B_l s^2 + (J_e K + K J_l) s + K B_l}$$

Sketching the Bode Plot for a Transfer Function (1/2)

Evaluate transfer function on imaginary axis

$$M = |G(i\omega)|, \quad \varphi = \arctan \frac{\text{Im } G(i\omega)}{\text{Re } G(i\omega)}$$

$$\log |G(i\omega)| \approx \begin{cases} 0 & \text{if } \omega < a \\ \log a - \log \omega & \text{if } \omega > a, \end{cases}$$

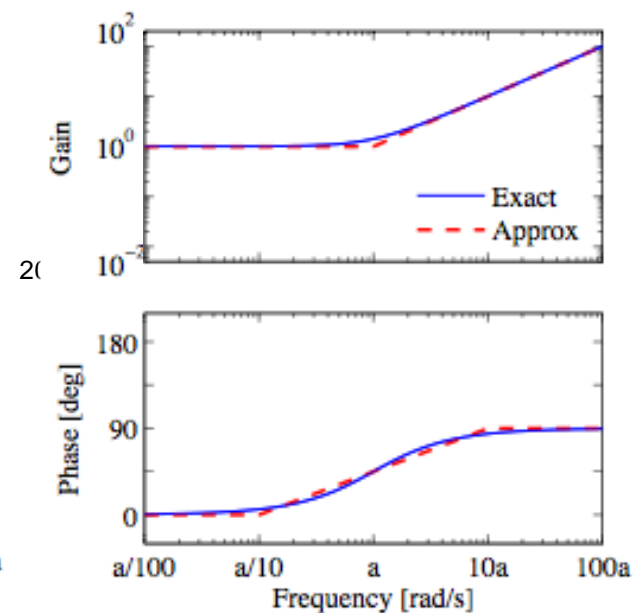
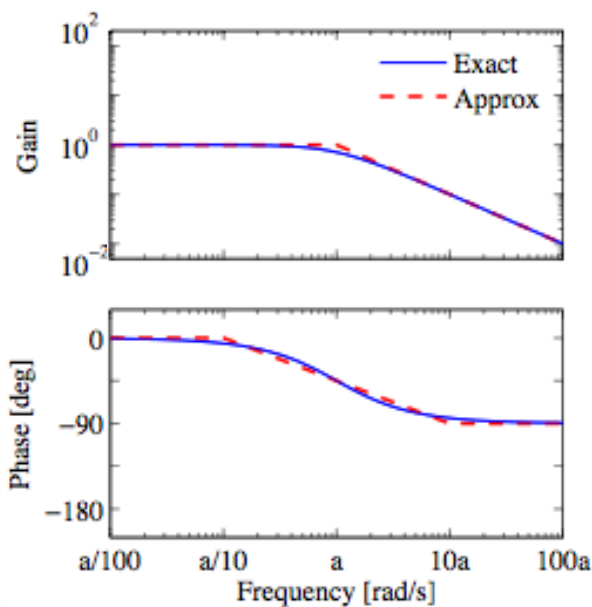
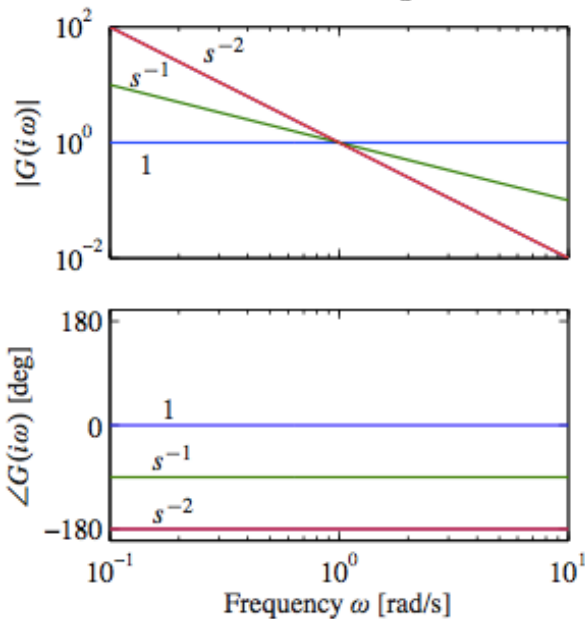
$$\angle G(i\omega) \approx \begin{cases} 0 & \text{if } \omega < a/10 \\ -45 - 45(\log \omega - \log a) & a/10 < \omega < 10a \\ -90 & \text{if } \omega > 10a. \end{cases}$$

- Plot gain (M) on log/log scale
- Plot phase (φ) on log/linear scale
- Piecewise linear approximations available

$$G(s) = \frac{1}{s^k}$$

$$G(s) = \frac{a}{s+a}$$

$$G(s) = \frac{s+a}{a}$$



Sketching the Bode Plot for a Transfer Function (2/2)

Complex poles $G(s) = \frac{\omega_0^2}{s^2 + 2\omega_0\zeta s + \omega_0^2}$

$$\log |G(i\omega)| \approx \begin{cases} 0 & \text{if } \omega \ll \omega_0 \\ 2 \log \omega_0 - 2 \log \omega & \text{if } \omega \gg \omega_0, \end{cases}$$

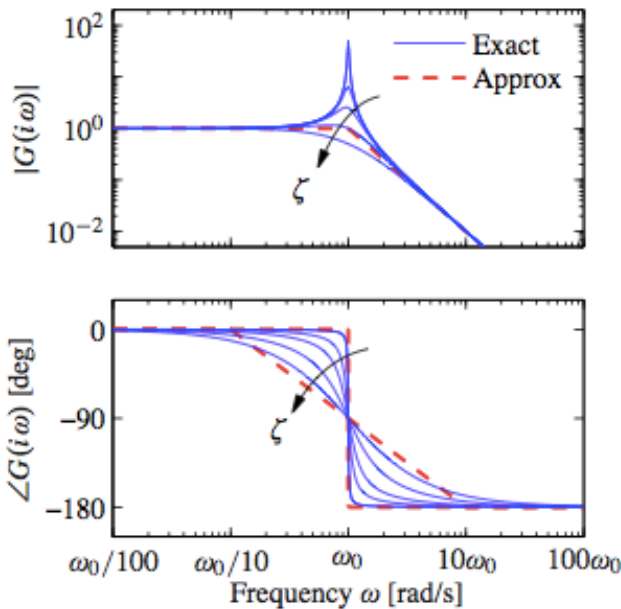
$$\angle G(i\omega) \approx \begin{cases} 0 & \text{if } \omega \ll \omega_0 \\ -180 & \text{if } \omega \gg \omega_0. \end{cases}$$

Ratios of products $G(s) = \frac{b_1(s)b_2(s)}{a_1(s)a_2(s)}$

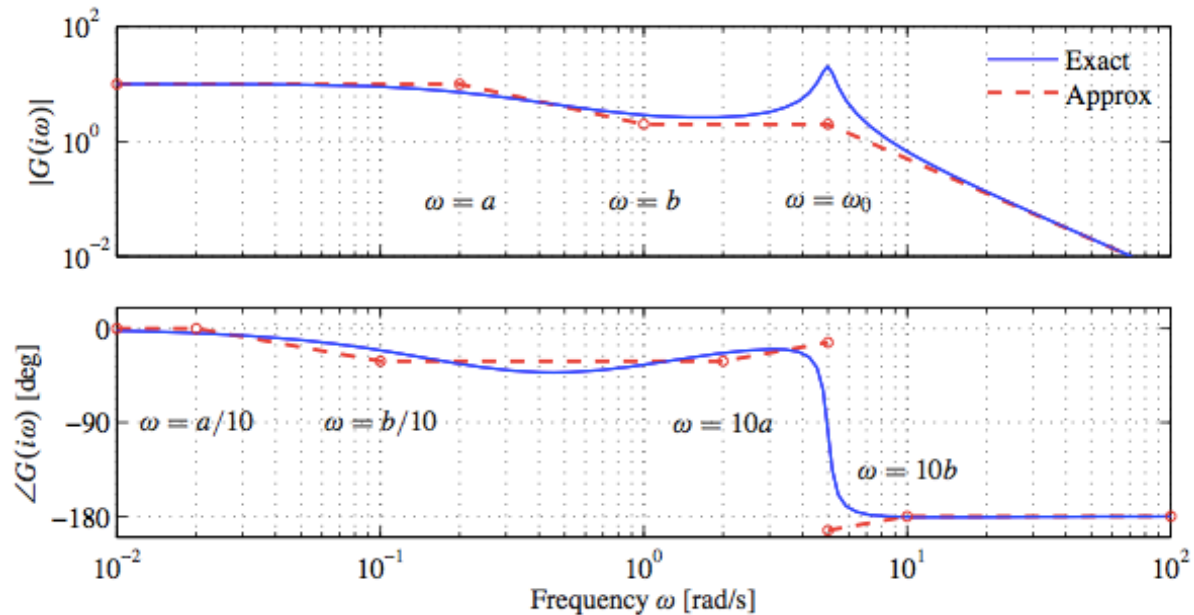
$$\log |G(s)| = \log |b_1(s)| + \log |b_2(s)| - \log |a_1(s)| - \log |a_2(s)|$$

$$\angle G(s) = \angle b_1(s) + \angle b_2(s) - \angle a_1(s) - \angle a_2(s)$$

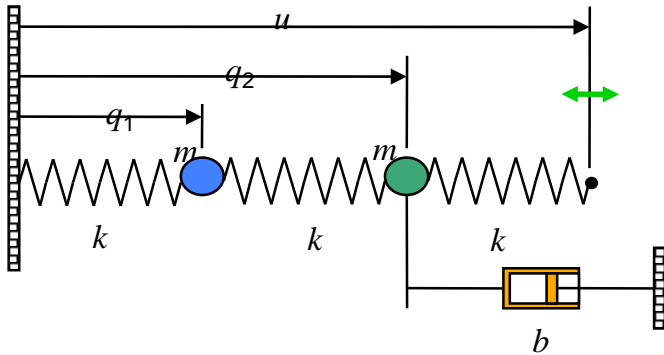
$$G(s) = \frac{\omega_0^2}{s^2 + 2\omega_0\zeta s + \omega_0^2}$$



$$G(s) = \frac{k(s+b)}{(s+a)(s^2 + 2\zeta\omega_0s + \omega_0^2)}, \quad a \ll b \ll \omega_0.$$



Example: Coupled Masses



$$H_{q_1f} = \frac{0.04}{s^4 + 0.08s^3 + 0.8016s^2 + 0.032s + 0.12}$$

$$H_{q_2f} = \frac{0.2s^2 + 0.008s + 0.08}{s^4 + 0.08s^3 + 0.8016s^2 + 0.032s + 0.12}$$

Poles (H_{q_1f} and H_{q_2f})

- $-0.0200 \pm 0.7743j$
- $-0.0200 \pm 0.4468j$

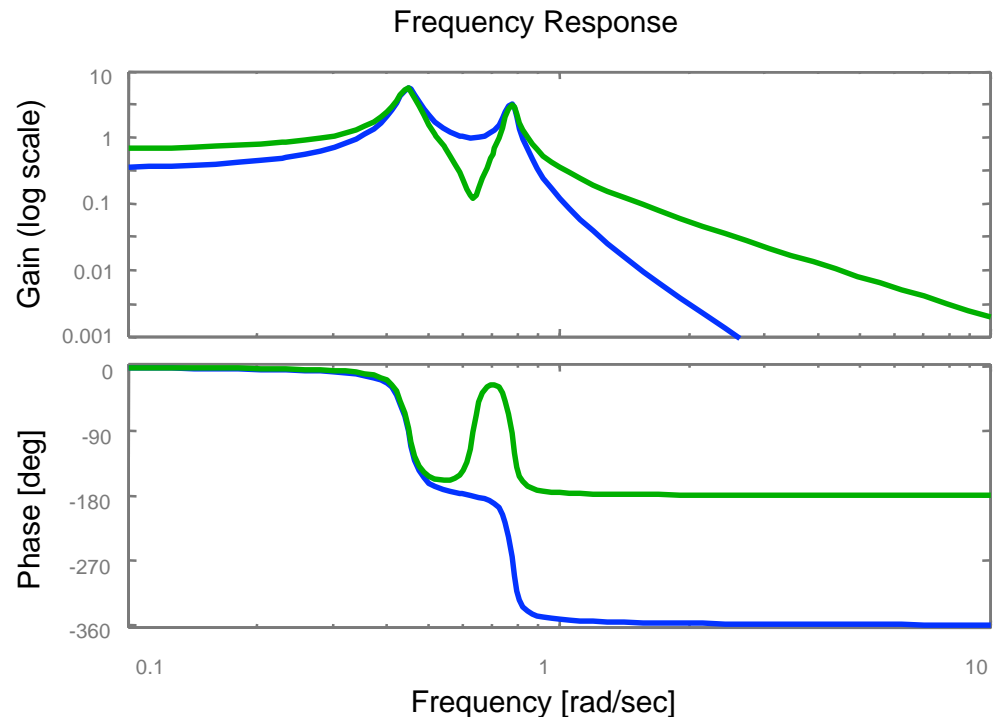
Zeros (H_{q_2f})

- $-0.0200 \pm 0.6321j$

Interpretation

- Zeros in H_{q_2f} give low response at $\omega \approx 0.6321$

MATLAB: `bode(H)`



MATLAB/Python manipulation of transfer functions

Creating transfer functions

- $[\text{num}, \text{den}] = \text{ss2tf}(A, B, C, D)$
- $\text{sys} = \text{tf}(\text{num}, \text{den})$
- $\text{num}, \text{den} = [1 \ a \ b] \rightarrow s^2 + as + b$

Interconnecting blocks

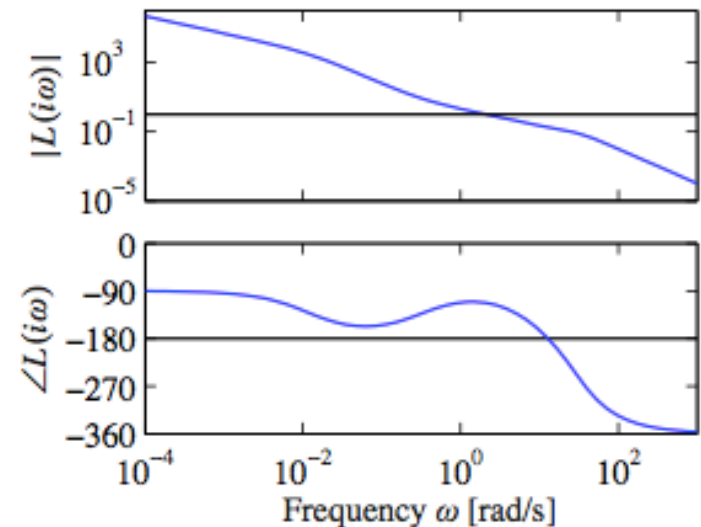
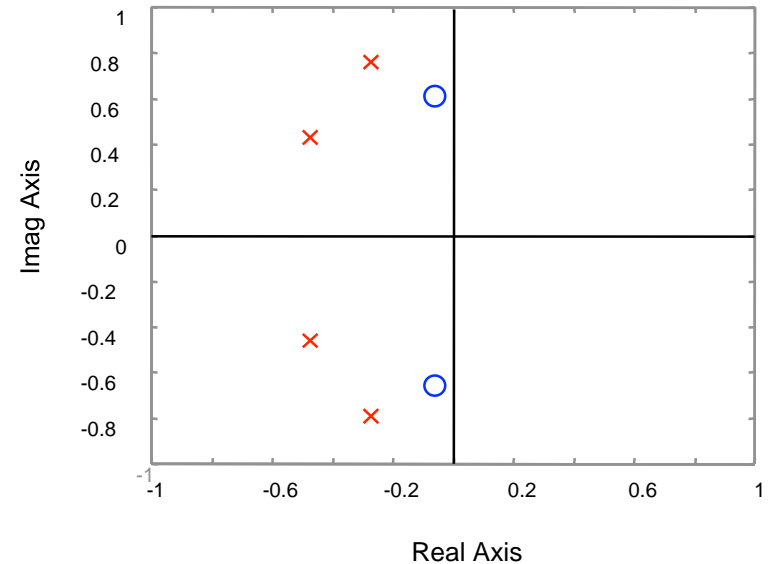
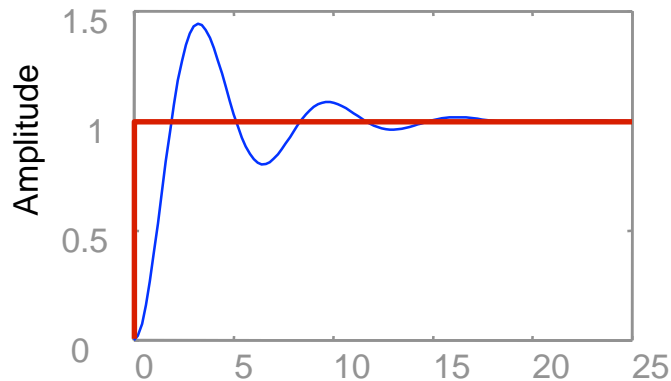
- $\text{sys} = \text{series}(\text{sys1}, \text{sys2})$, parallel, feedback

Computing poles and zeros

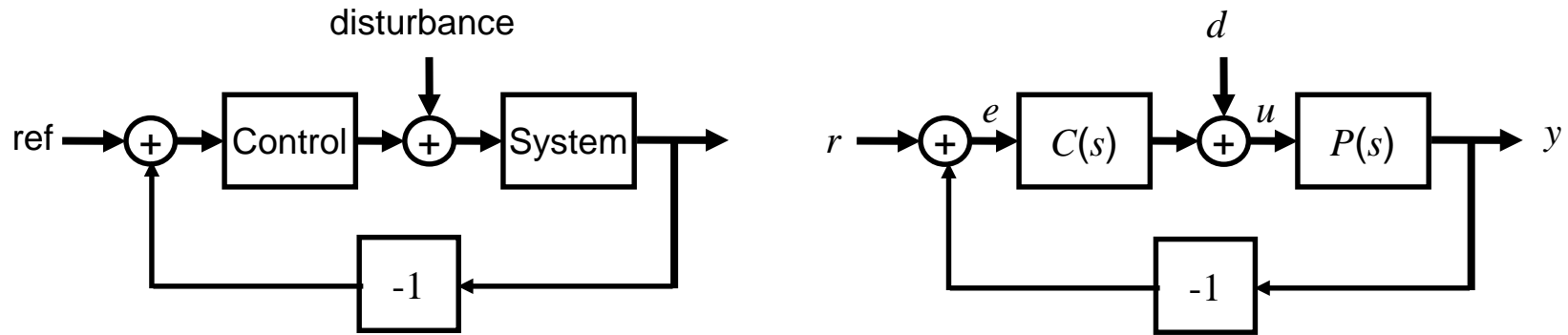
- $\text{pole}(\text{sys})$, $\text{zero}(\text{sys})$
- $\text{pzmap}(\text{sys})$

I/O response

- $\text{initial}(\text{sys})$
- $\text{step}(\text{sys})$
- $\text{lsim}(\text{sys})$
- $\text{bode}(\text{sys})$



Control Analysis and Design Using Transfer Functions



Transfer functions provide a method for “block diagram algebra”

- Easy to compute transfer functions between various inputs and outputs
 - $H_{er}(s)$ is the transfer function between the reference and the error
 - $H_{ed}(s)$ is the transfer function between the disturbance and the error

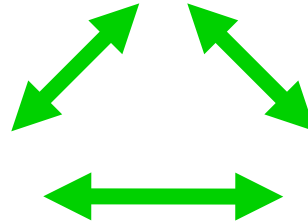
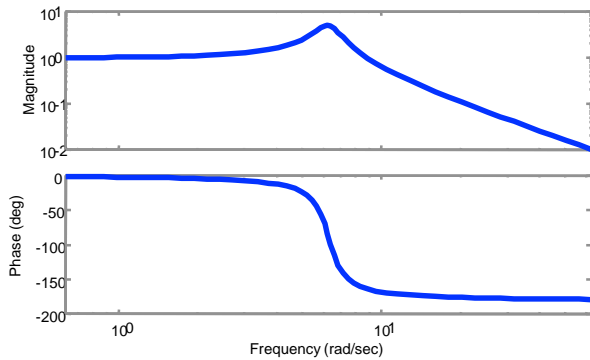
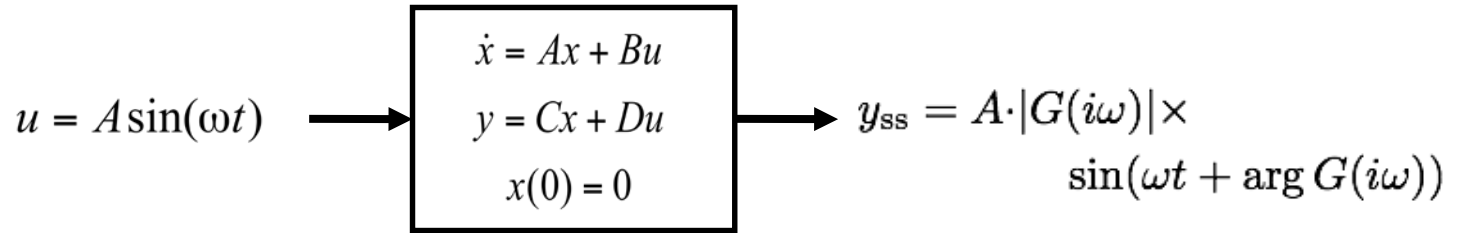
Transfer functions provide a method for performance specification

- Since transfer functions provide frequency response directly, it is convenient to work in the “frequency domain”
 - $H_{er}(s)$ should be small in the frequency range 0 to 10 Hz (good tracking)

Key idea: perform all analysis and design for linear systems in “frequency domain”

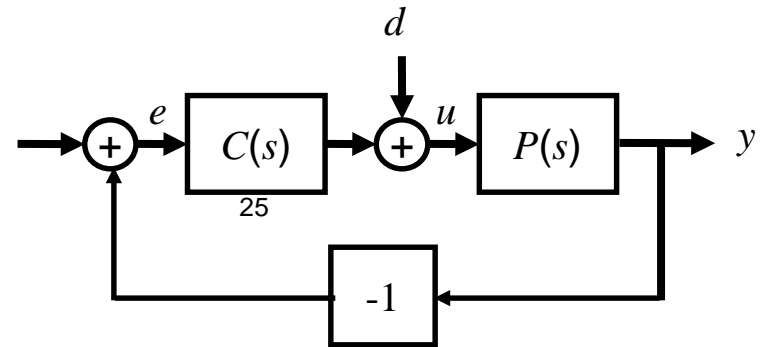
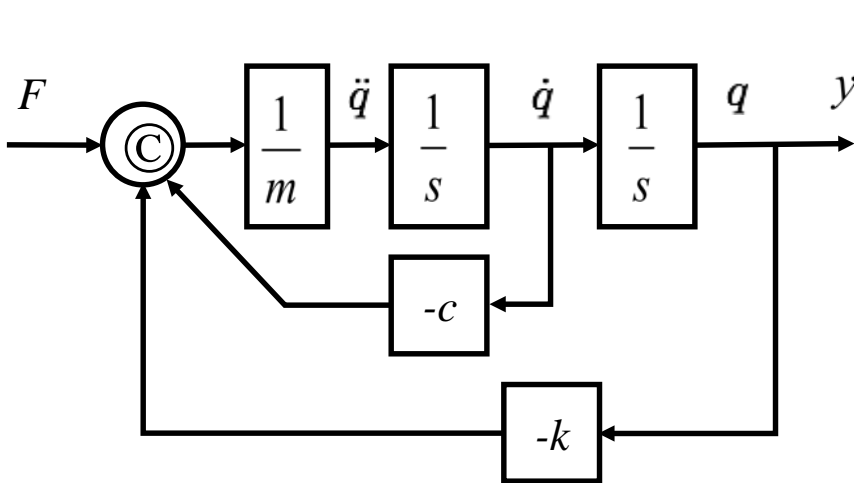
- Convert specifications on time response to specifications on frequency response
- “Shape” the frequency response by design of controller transfer function (Ch 10-13)

Summary: Frequency Response & Transfer Functions

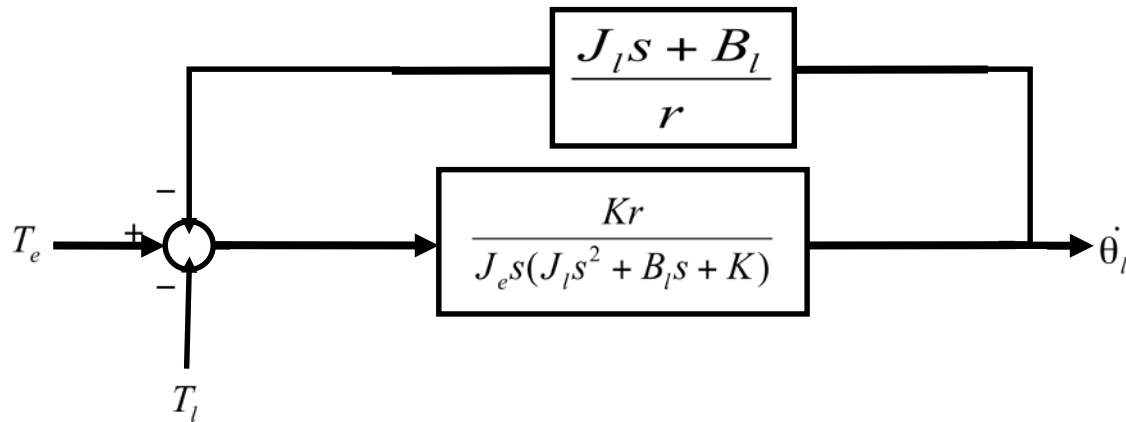
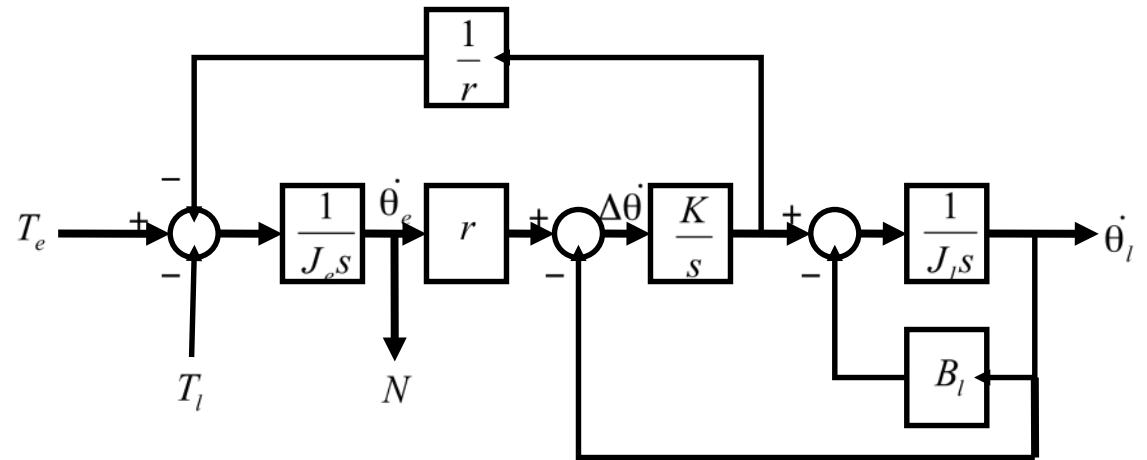


$$G(s) = C(sI - A)^{-1}B + D$$

$$G_{y_2 u_1} = G_{y_2 u_2} G_{y_1 u_1} = \frac{n_1 n_2}{d_1 d_2}$$

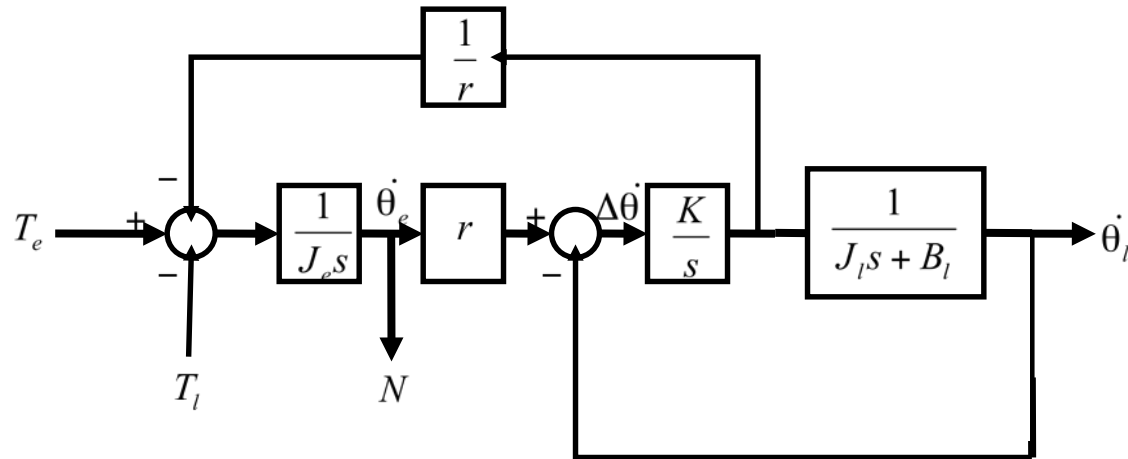
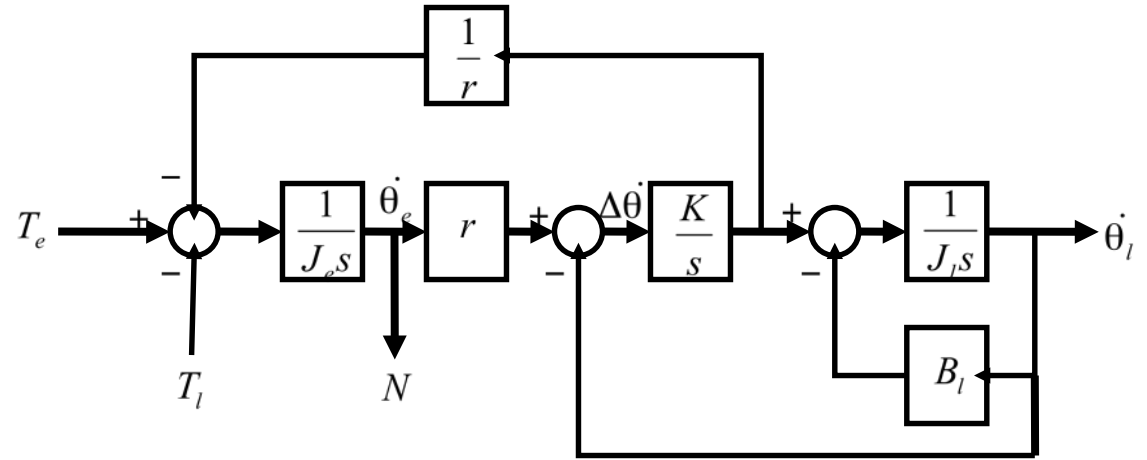


Example: Engine Control of a GM Astro

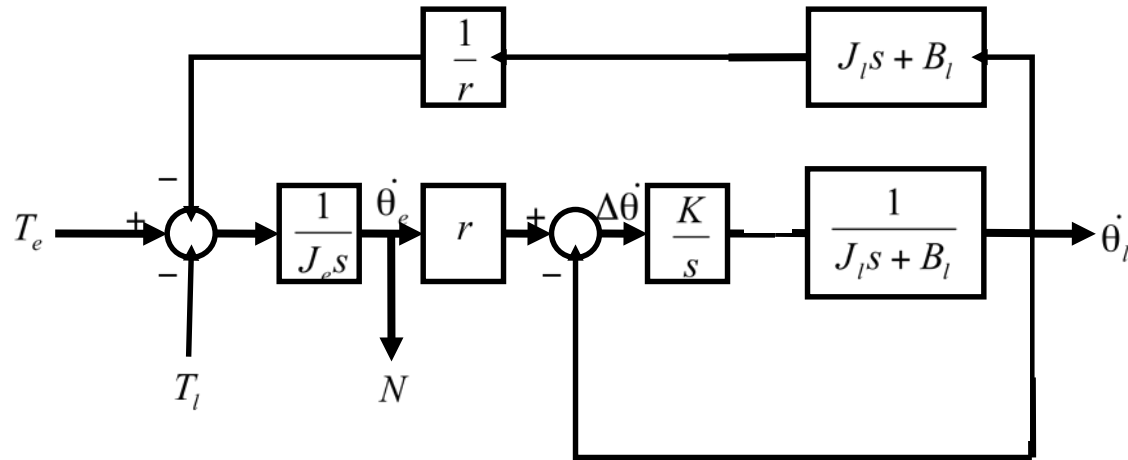
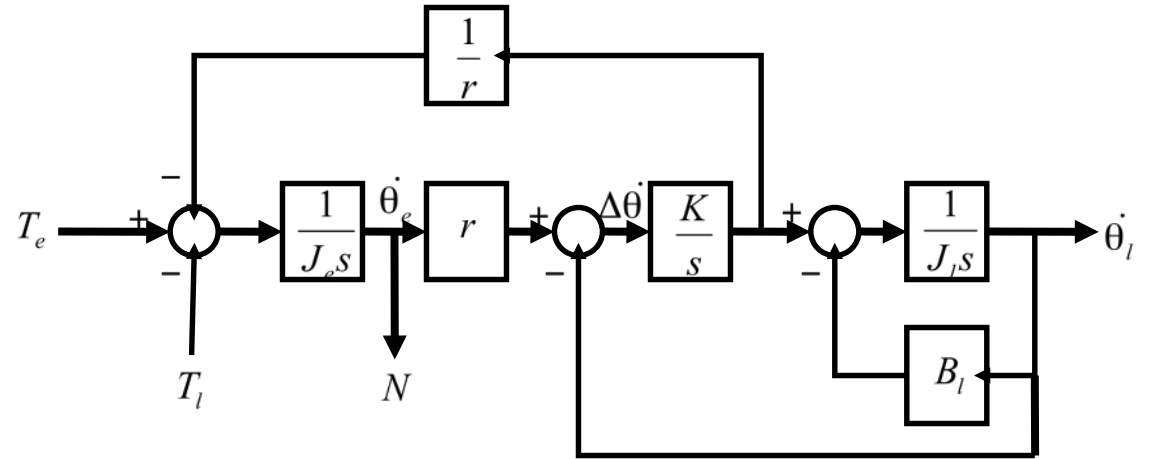


$$H_{\theta_l T_e}(s) = \frac{Kr}{J_e J_l s^3 + J_e B_l s^2 + (J_e K + K J_l) s + K B_l}$$

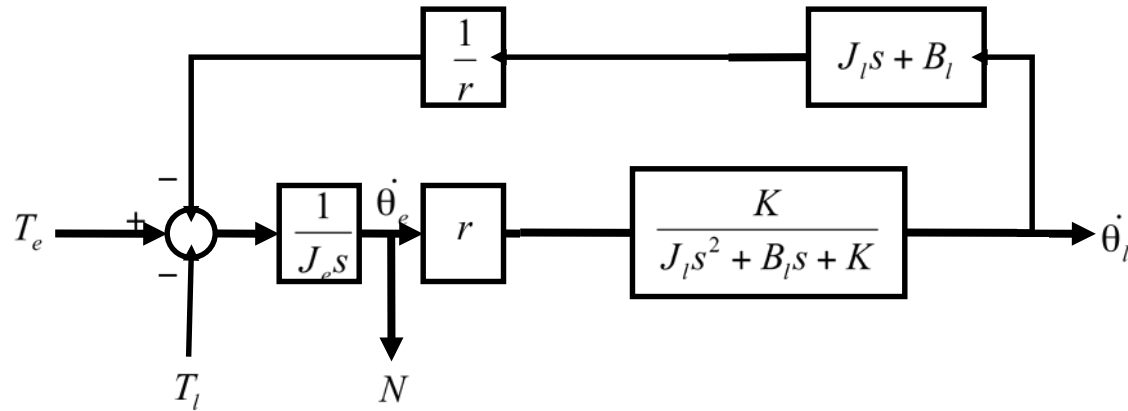
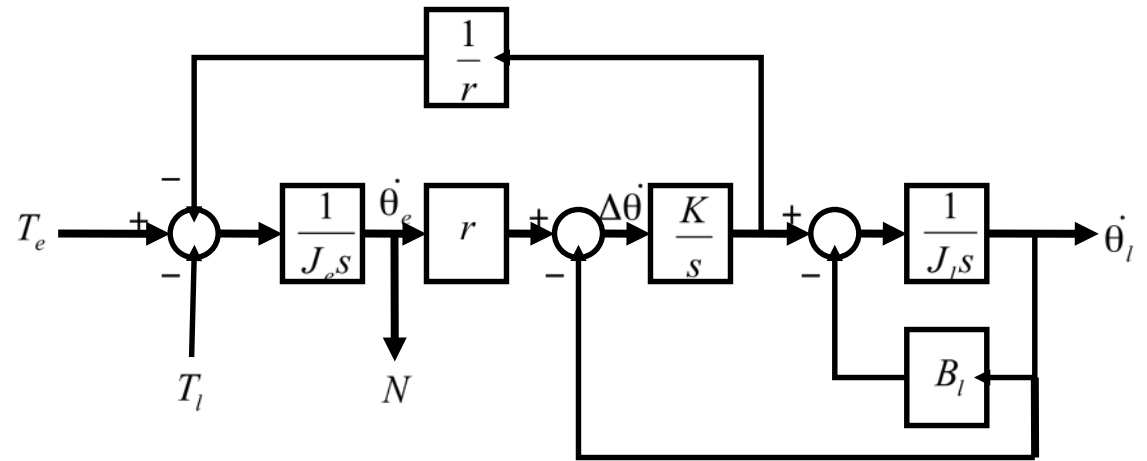
Example: Engine Control of a GM Astro



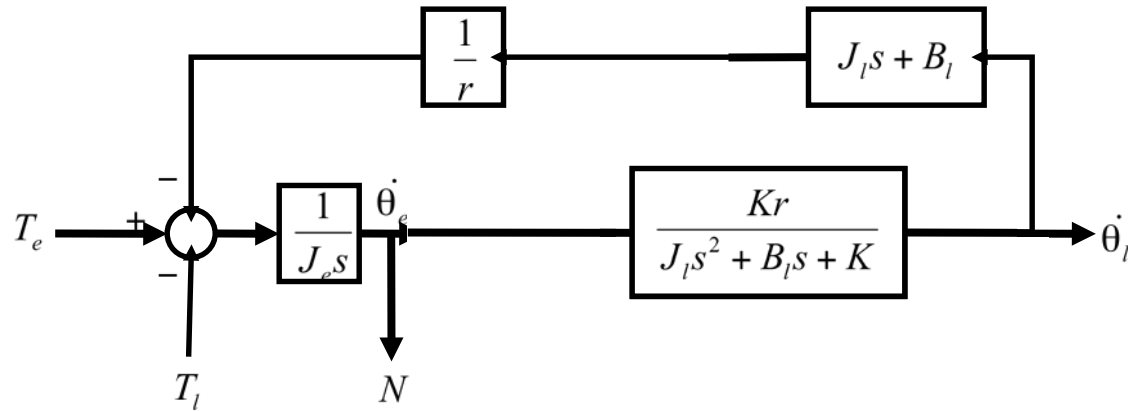
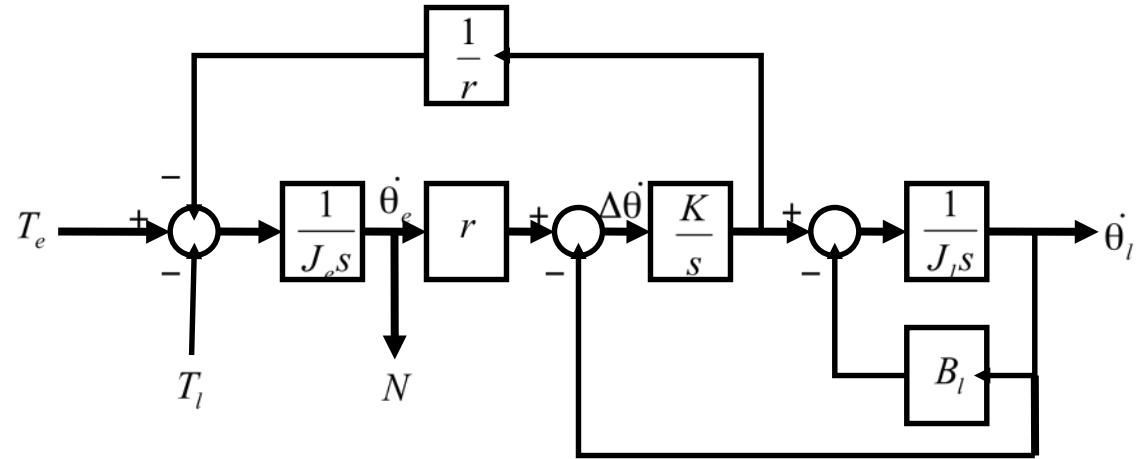
Example: Engine Control of a GM Astro



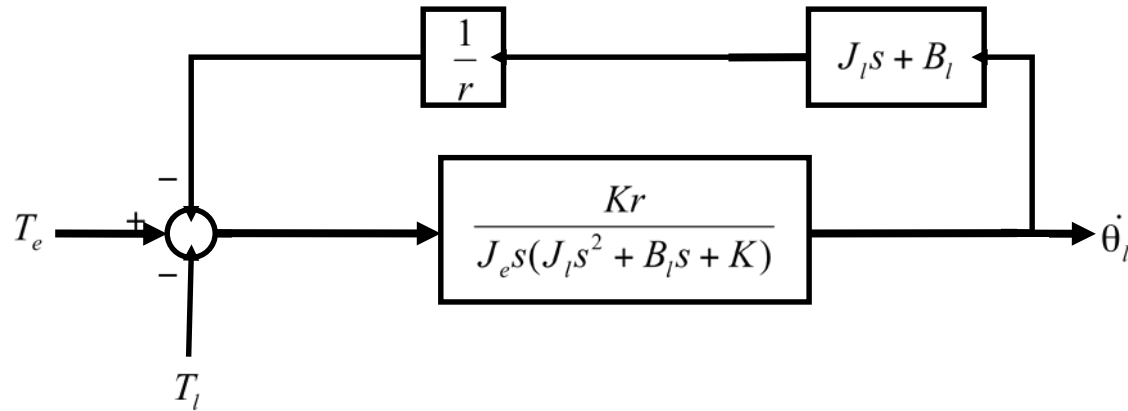
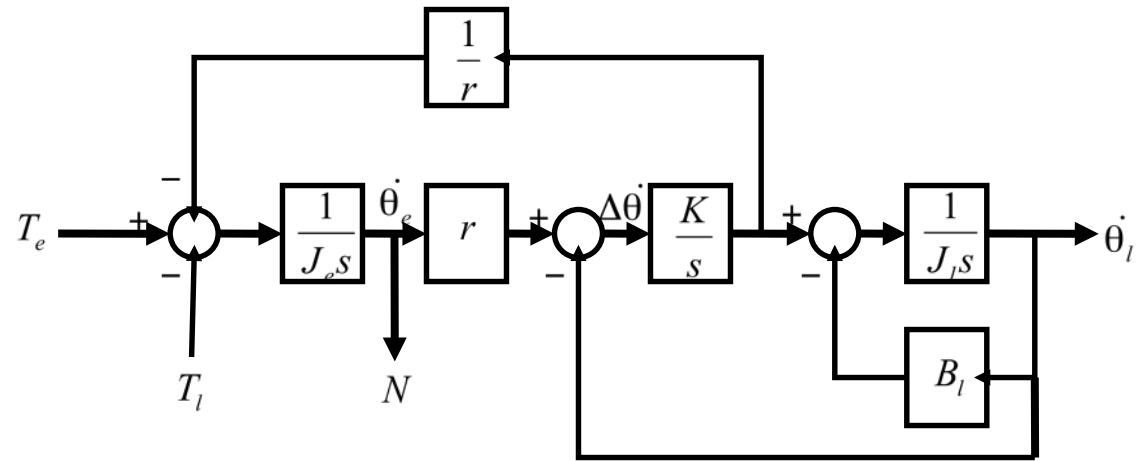
Example: Engine Control of a GM Astro



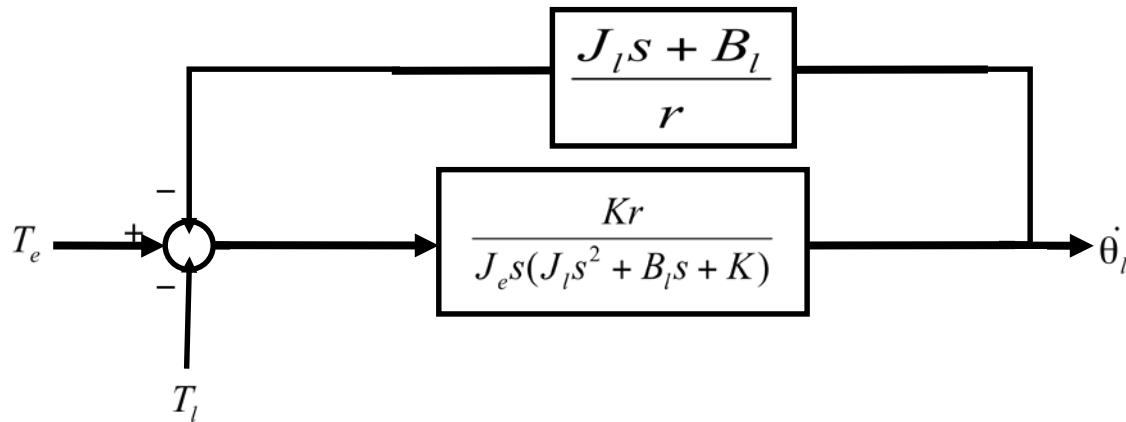
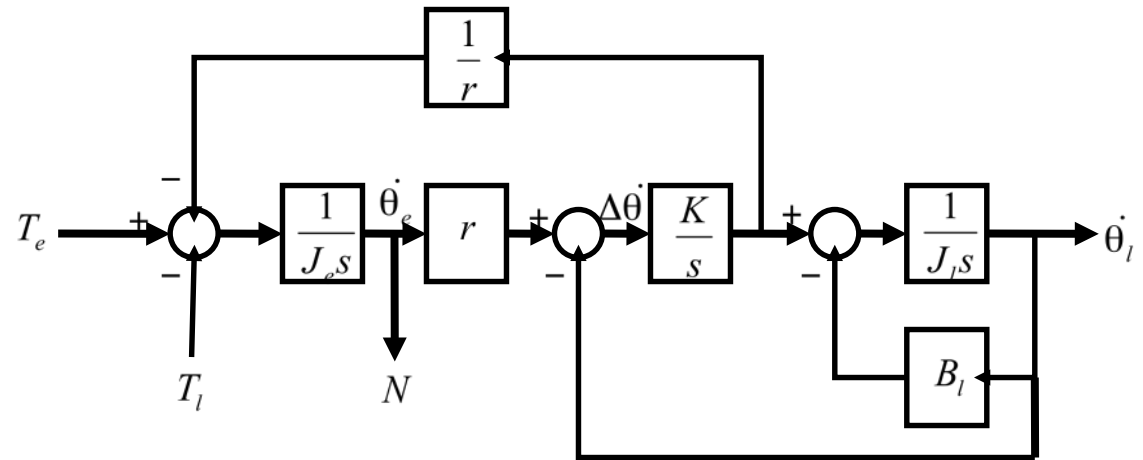
Example: Engine Control of a GM Astro



Example: Engine Control of a GM Astro



Example: Engine Control of a GM Astro



$$H_{\theta_l T_e}(s) = \frac{Kr}{J_e J_l s^3 + J_e B_l s^2 + (J_e K + K J_l) s + K B_l}$$