



# CDS 101/110: Lecture 7.2

## Loop Analysis of Feedback Systems



**November 11 2016**

### **Goals:**

- Why Nyquist Diagrams?
- *Gain margin and phase margin*
- Examples!

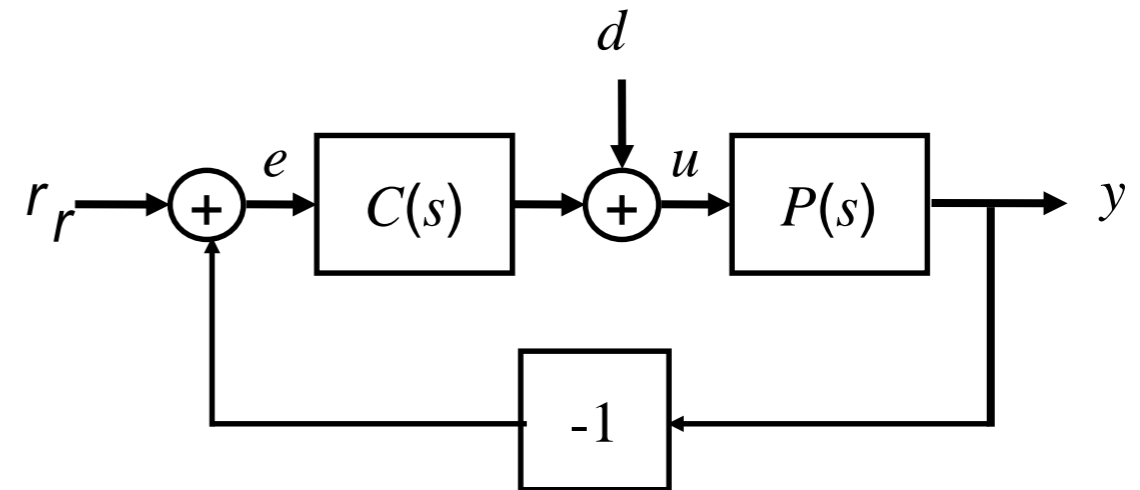
### **Reading:**

- Åström and Murray, Feedback Systems, Chapter 10, Sections 10.1-10.4,

# What can you do with a Nyquist Analysis?

## Set Up (somewhat artificial):

- **Given:**  $P(s)$ 
  - (any unstable roots known)
- **Given:**  $C(s)$ 
  - (any unstable roots known)
- **Q:** can negative output feedback stabilize the system (stable  $G_{yr}(s)$ )?



## Possible Solutions:

$$G_{yr}(s) = \frac{PC}{1+PC} = \frac{n_p(s)n_c(s)}{d_p(s)d_c(s)+n_p(s)n_c(s)}$$

- Compute and check poles of  $G_{yr}$
- Find another way to determine existence of unstable poles without computing roots of

$$d_p(s)d_c(s) + n_p(s)n_c(s)$$

## The Nyquist plot *logic*

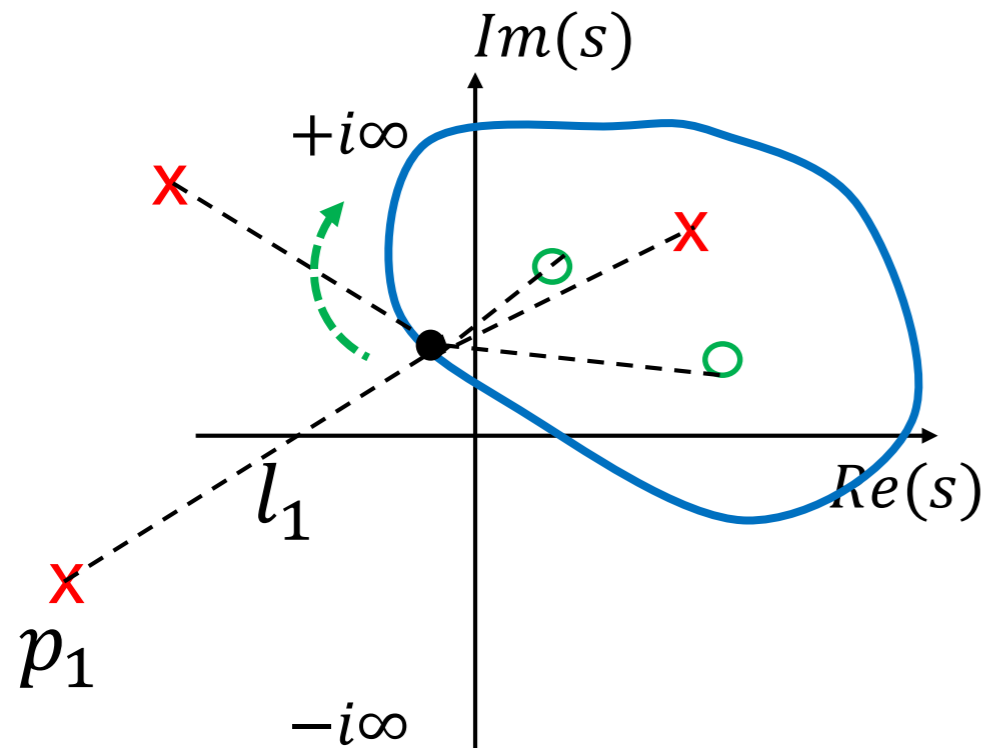
- Poles of  $G_{yr}(s)$  are zeros of

$$1 + P(s)C(s) = \frac{d_p(s)d_c(s) + n_p(s)n_c(s)}{d_p(s)d_c(s)}$$

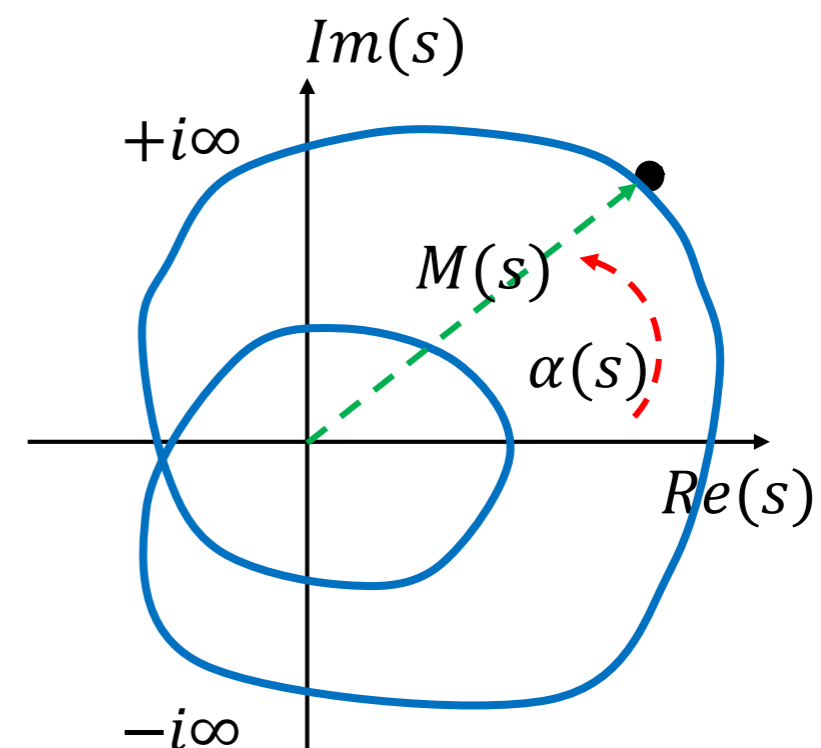
- If  $G_{yr}(s)$  is unstable, then it has at least one pole in RHP
- An unstable pole of  $G_{yr}(s)$  implies and unstable (RHP) zero of  $1 + P(s)C(s)$
- Nyquist plot and Nyquist Criterion allow us to determine if  $1 + PC$  has RHP zeros *without* polynomial solving.

# Argument Principle

(underlying Nyquist Criterion)



$L(s)$



$$f(s) = \frac{(s - z_1)(s - z_2) \cdots (s - z_m)}{(s - p_1)(s - p_2) \cdots (s - p_n)} = \frac{r_1(s)e^{i\psi_1(s)} r_2(s)e^{i\psi_2(s)} \cdots r_m(s)e^{i\psi_m(s)}}{l_1(s)e^{i\phi_1(s)} l_2(s)e^{i\phi_2(s)} \cdots l_n(s)e^{i\phi_n(s)}}$$

$$= M(s)e^{i\alpha}$$

$$\alpha(s) = \sum_{i=1}^m \psi_i(s) - \sum_{j=1}^n \phi_j(s)$$

As  $s$  moves *clockwise* around  $\Gamma$ ,  $L(s)$  must rotate around the origin by  $2\pi$  for each pole inside the contour, and by  $-2\pi$  for each zero inside the contour

- $P$  # RHP poles of open loop  $L(s)$  (from  $P(s), C(s)$  poles)
- $N$  # clockwise encirclements of  $-1$  (from Nyquist plot)
- $Z$  # RHP zeros of  $1 + L(s)$

Then  $Z_{RHP} = N + P$

# Robust stability: gain and phase margins

Nyquist plot tells us if closed loop is stable, but not how stable

## Gain margin

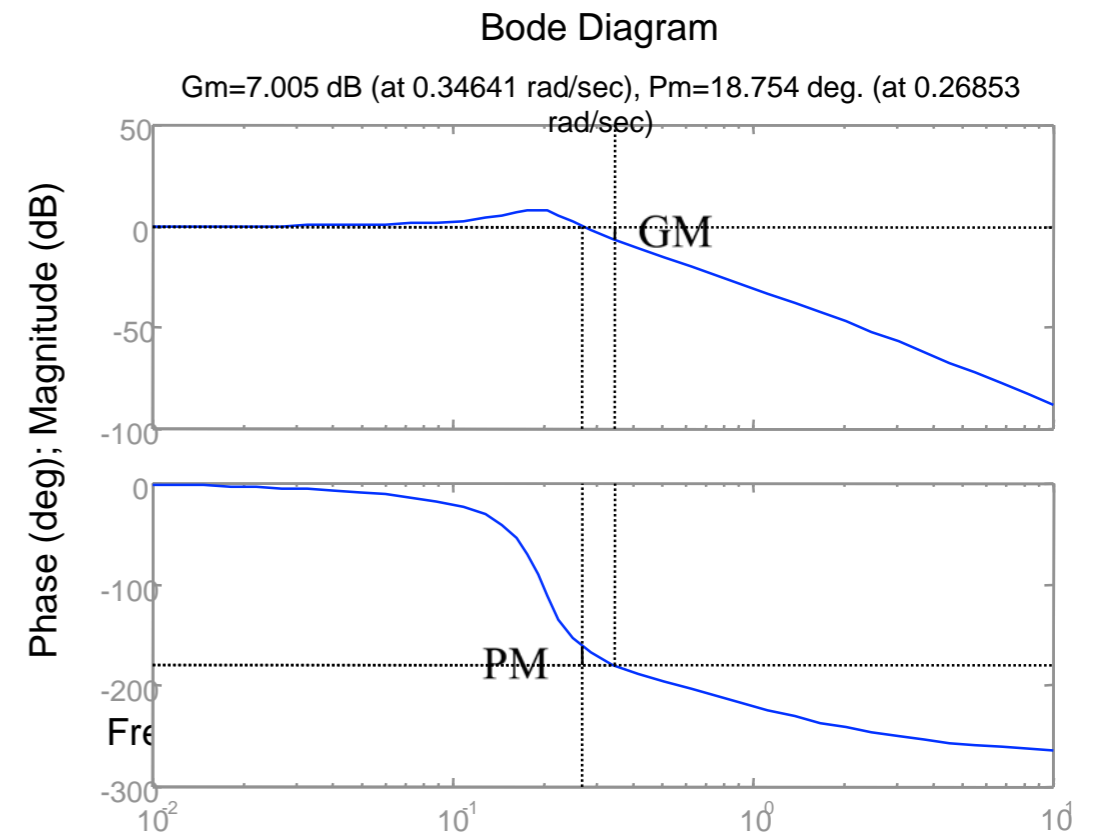
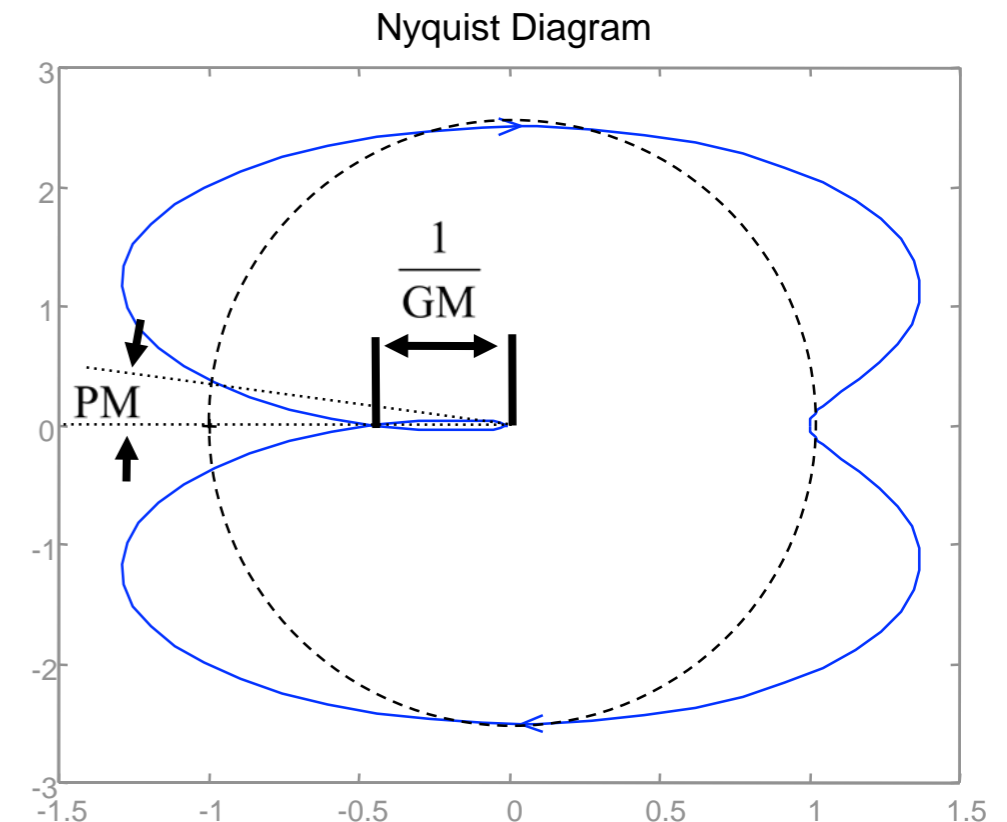
- How much we can modify the loop gain and still have the system be stable
- Determined by the location where the loop transfer function crosses  $180^\circ$  phase

## Phase margin

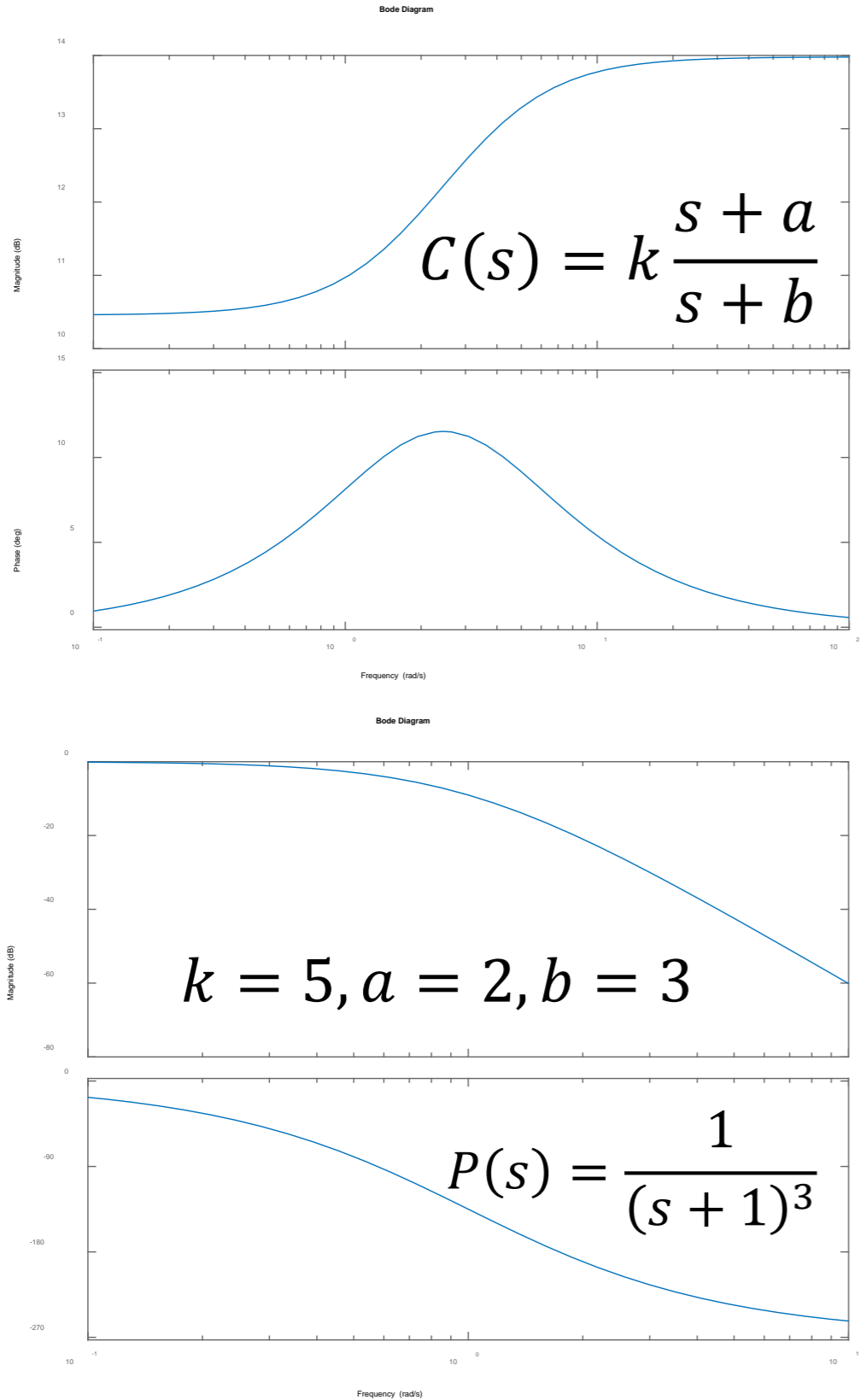
- How much “phase delay” can be added while system remains stable
- Determined by the phase at which the loop transfer function has unity gain

## Bode plot interpretation

- Look for gain = 1,  $180^\circ$  phase crossings
- MATLAB: `margin(sys)`



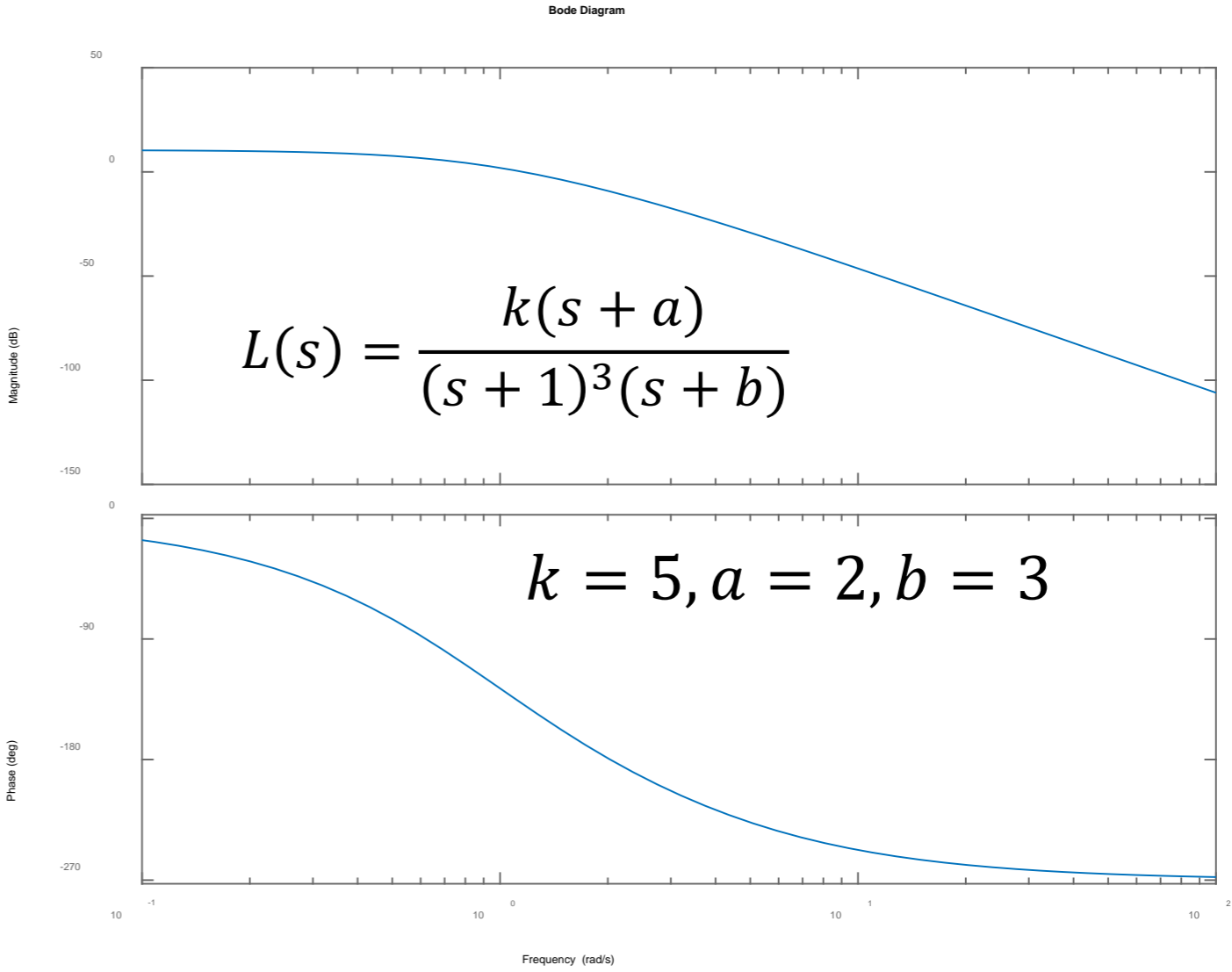
# Nyquist Plot Example #1



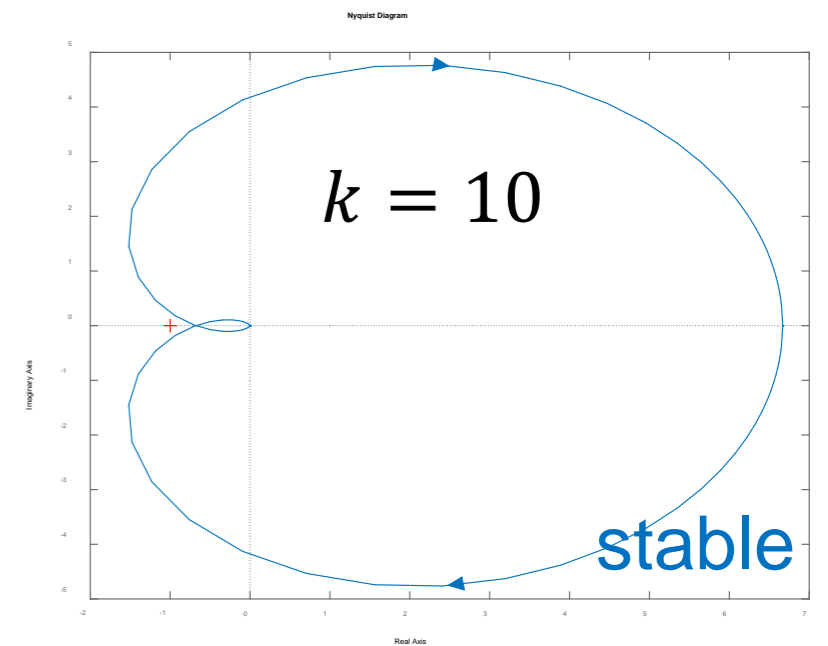
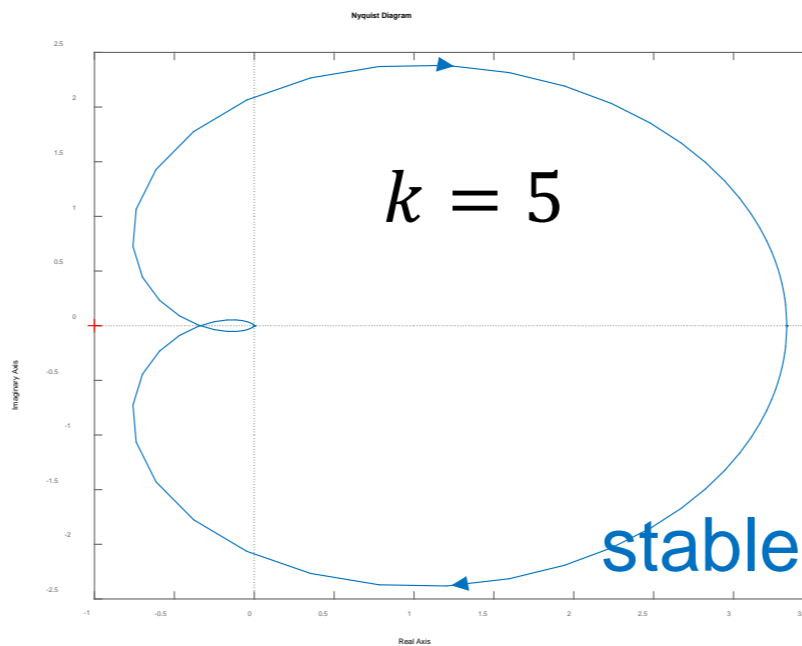
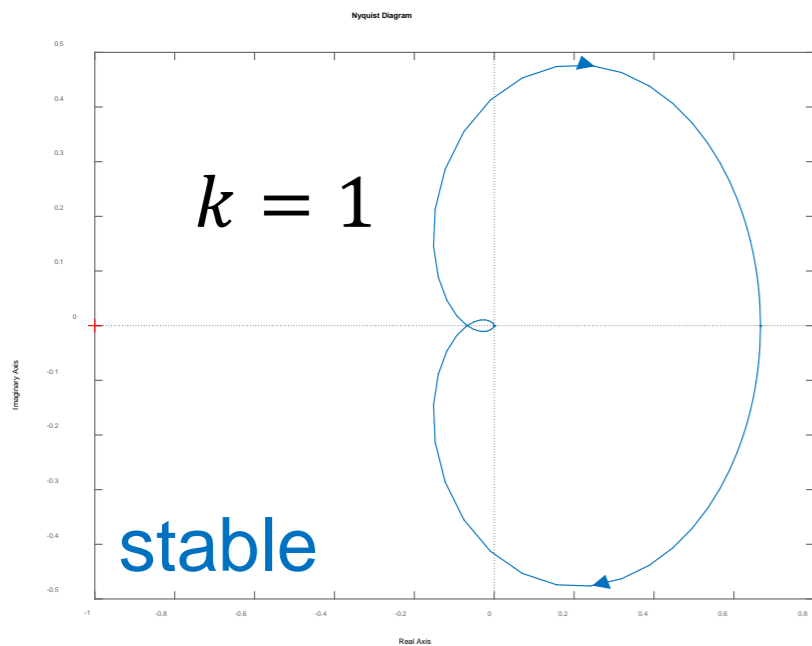
$$P(s) = \frac{1}{(s+1)^3} \quad C(s) = k \frac{s+a}{s+b}$$

$$1 < a < b$$

**Goal #1:** Is closed loop system stable?  
**Goal #2:** Does stability vary with gain?



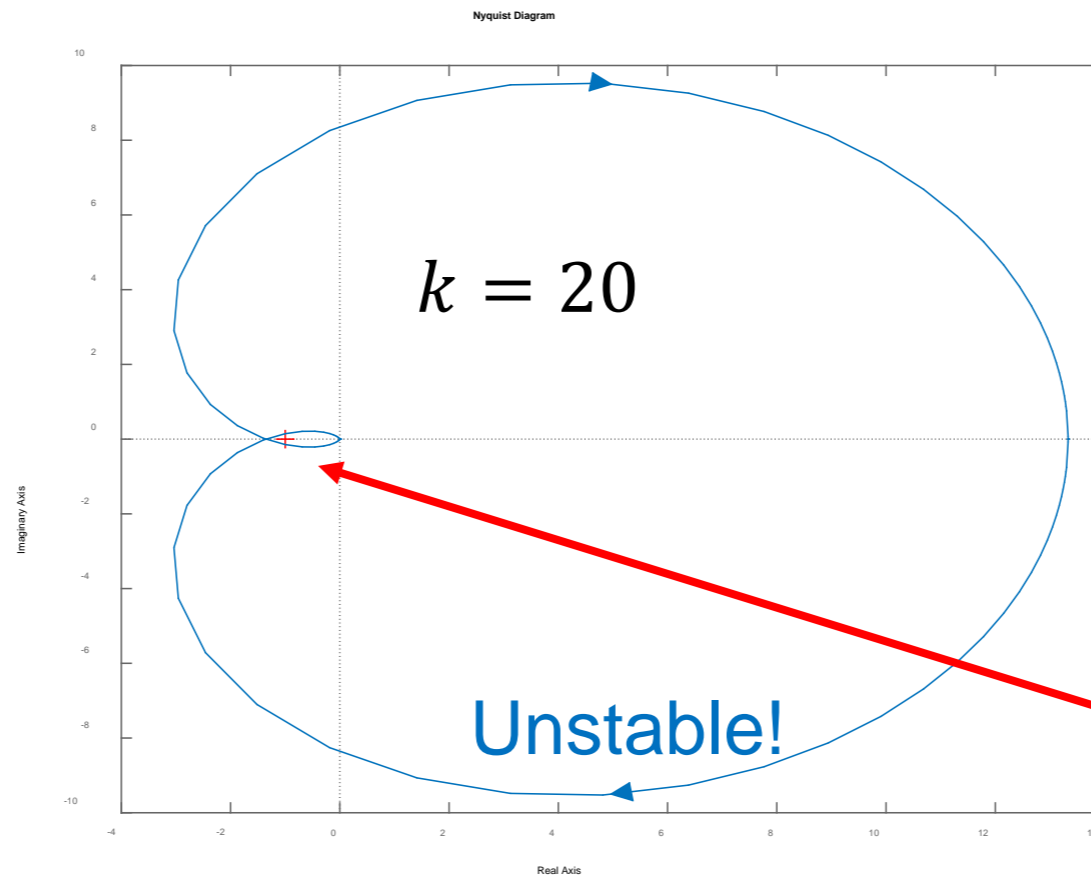
# Nyquist Plot Example #1



$$P(s) = \frac{1}{(s+1)^3}$$

$$C(s) = k \frac{s+a}{s+b}$$

$$1 < a < b$$



Nyquist:

- $P = 0$
- $N = +2$
- $Z_{RHP} = 2$

2 Encirclements  
of -1 point

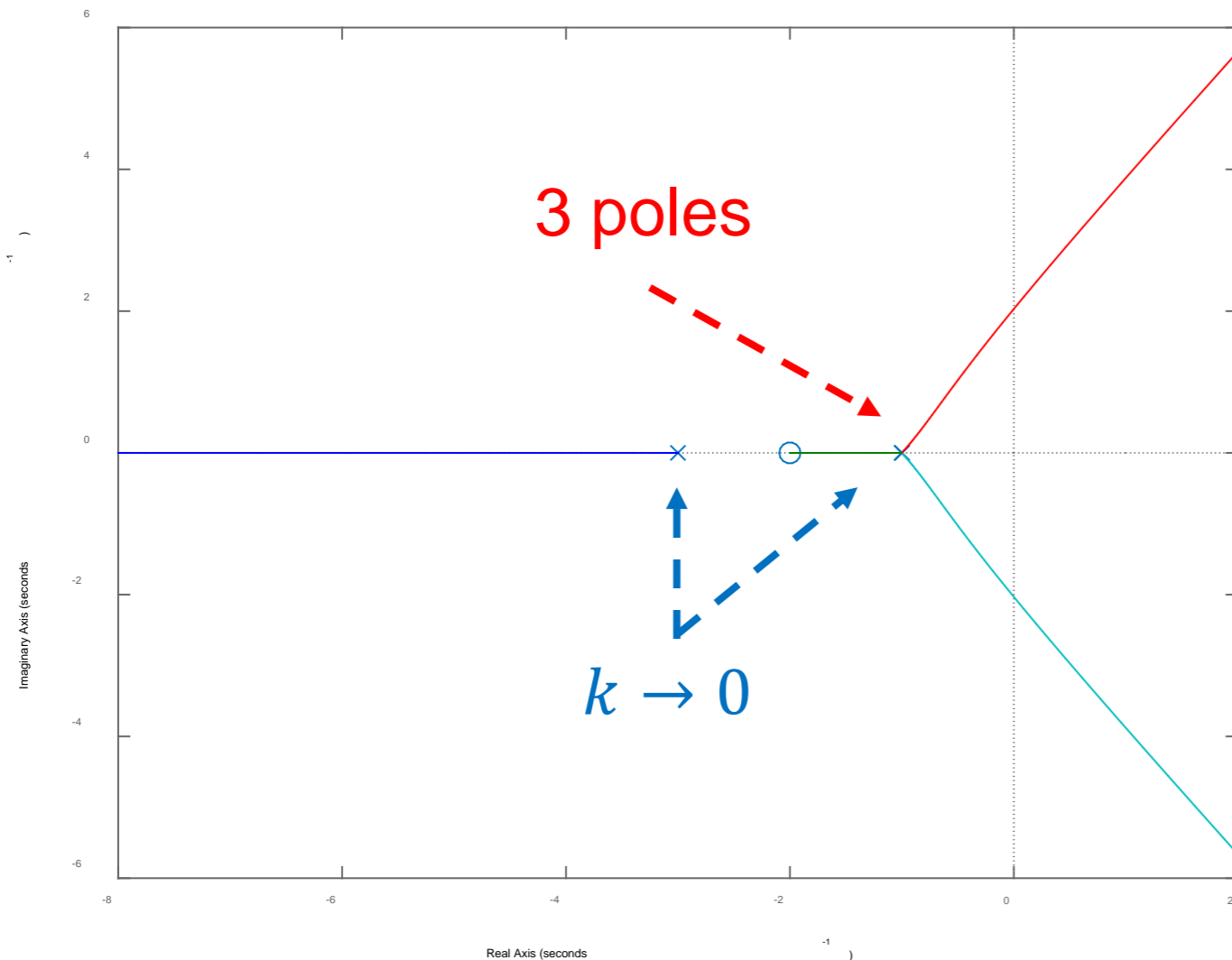
# Nyquist Plot Example #1

(alternative analysis without Nyquist)

$$L(s) = \frac{n_P(s)n_C(s)}{d_P(s)d_C(s)} = k \frac{n_P(s)n_{C'}(s)}{d_P(s)d_{C'}(s)} = k \frac{1}{(s+1)^3} \frac{s+a}{s+b}$$

$$G_{yr}(s) = \frac{P(s)C(s)}{1+P(s)C(s)} = \frac{kP(s)C'(s)}{1+kP(s)C'(s)} = \frac{k n_P(s)n_{C'}(s)}{d_P(s)d_{C'} + k n_P(s)n_{C'}(s)}$$

Root Locus



The **Root Locus** studies how the poles of  $G_{yr}(s)$  vary with  $k$

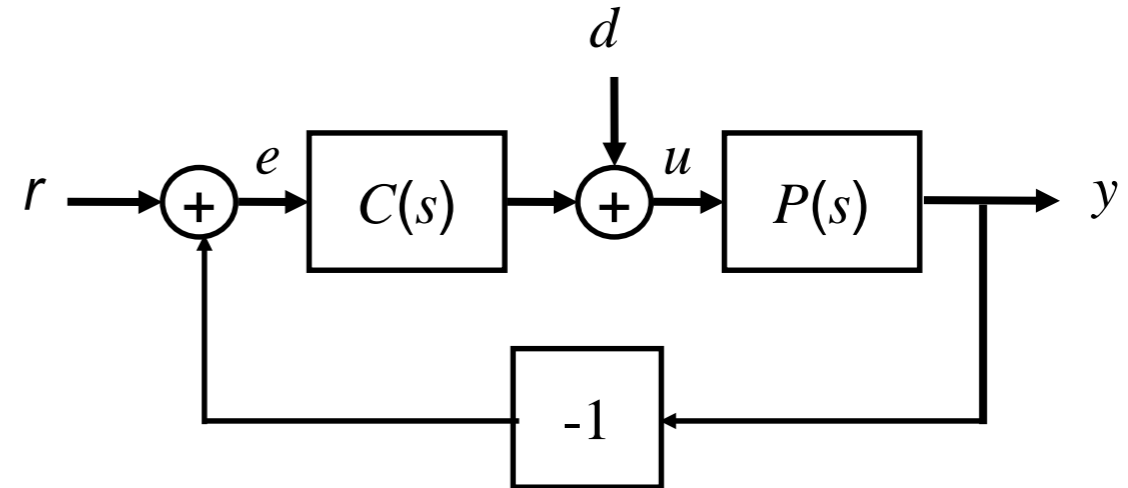
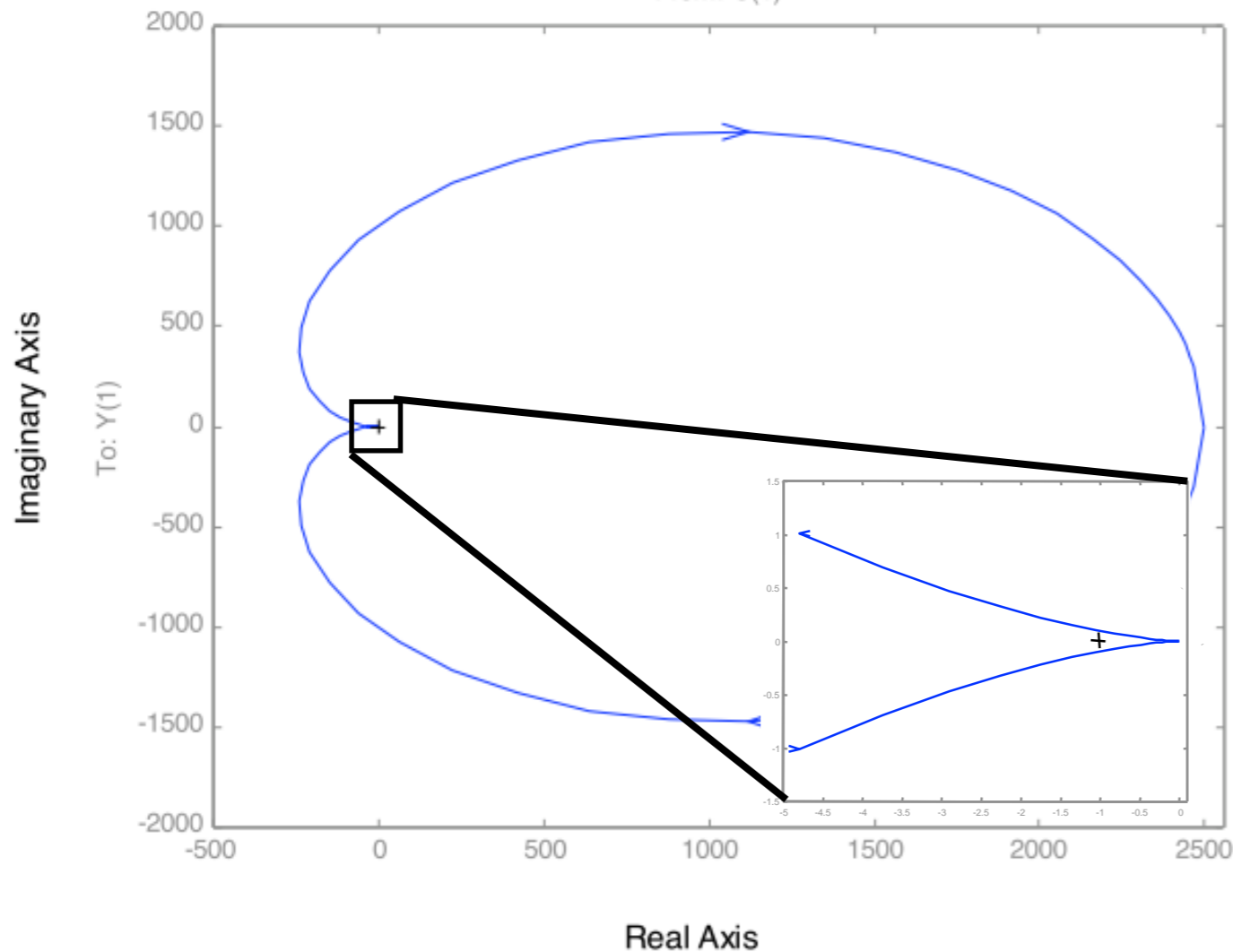
- When  $k \rightarrow 0$ , the poles of  $G_{yr}(s)$  approach the poles of  $L(s)$
- As  $k \rightarrow \infty$ , the poles of  $G_{yr}(s)$  approach the zeros of  $L(s)$  (or infinity)

For this problem, as  $k$  increases, two of the poles of  $G_{yr}(s)$  become unstable.

# Example: Proportional + Integral\* speed controller



Nyquist Diagrams  
From: U(1)



$$P(s) = \frac{1/m}{s + b/m} \times \frac{r}{s + a}$$

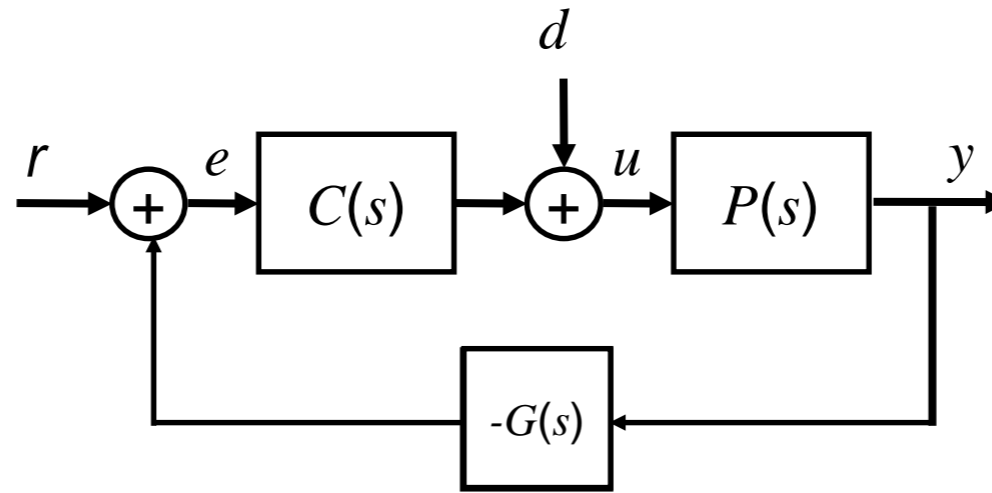
$$C(s) = K_p + \frac{K_i}{s + 0.01}$$

## Remarks

- $N = 0, P = 0 \Rightarrow Z = 0$  (stable)
- Need to zoom in to make sure there are no net encirclements
- Note that we don't have to compute closed loop response



# Example: cruise control



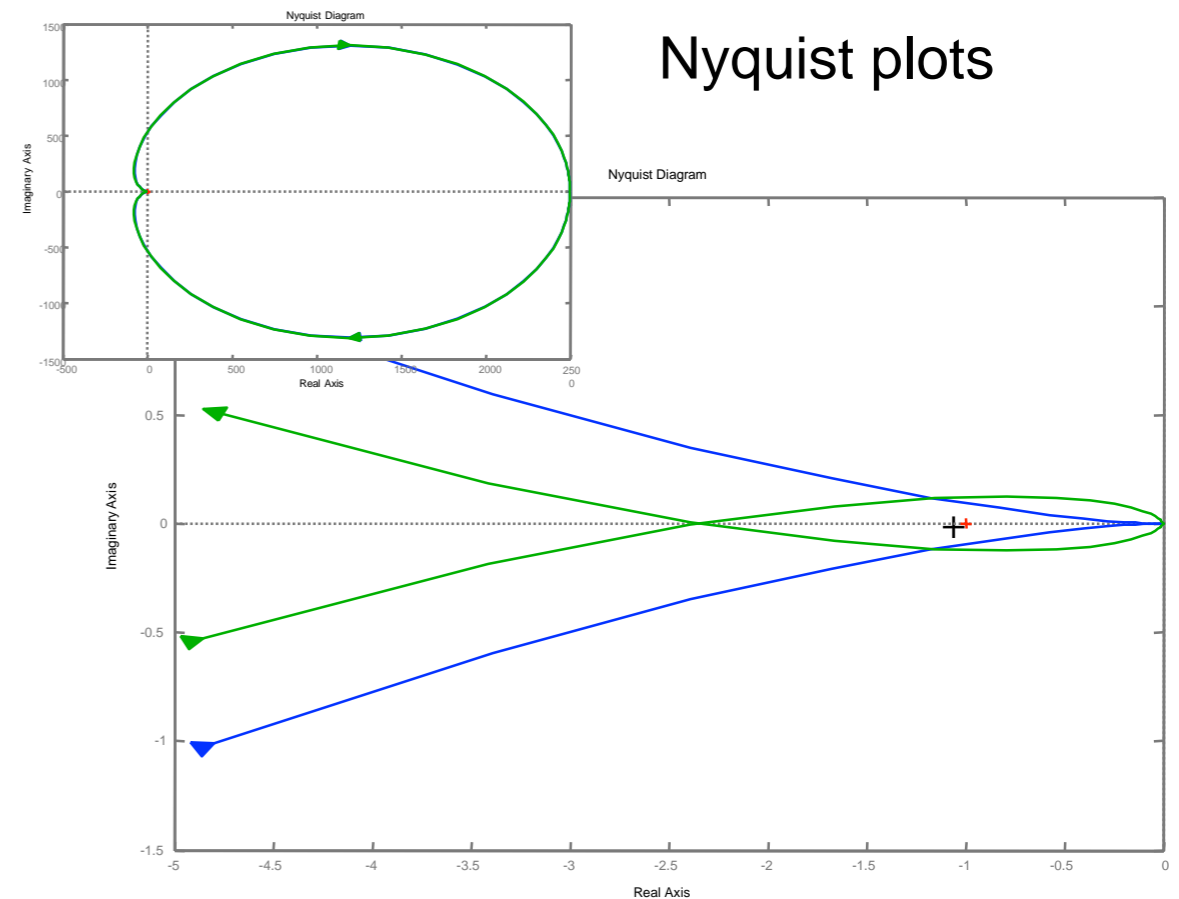
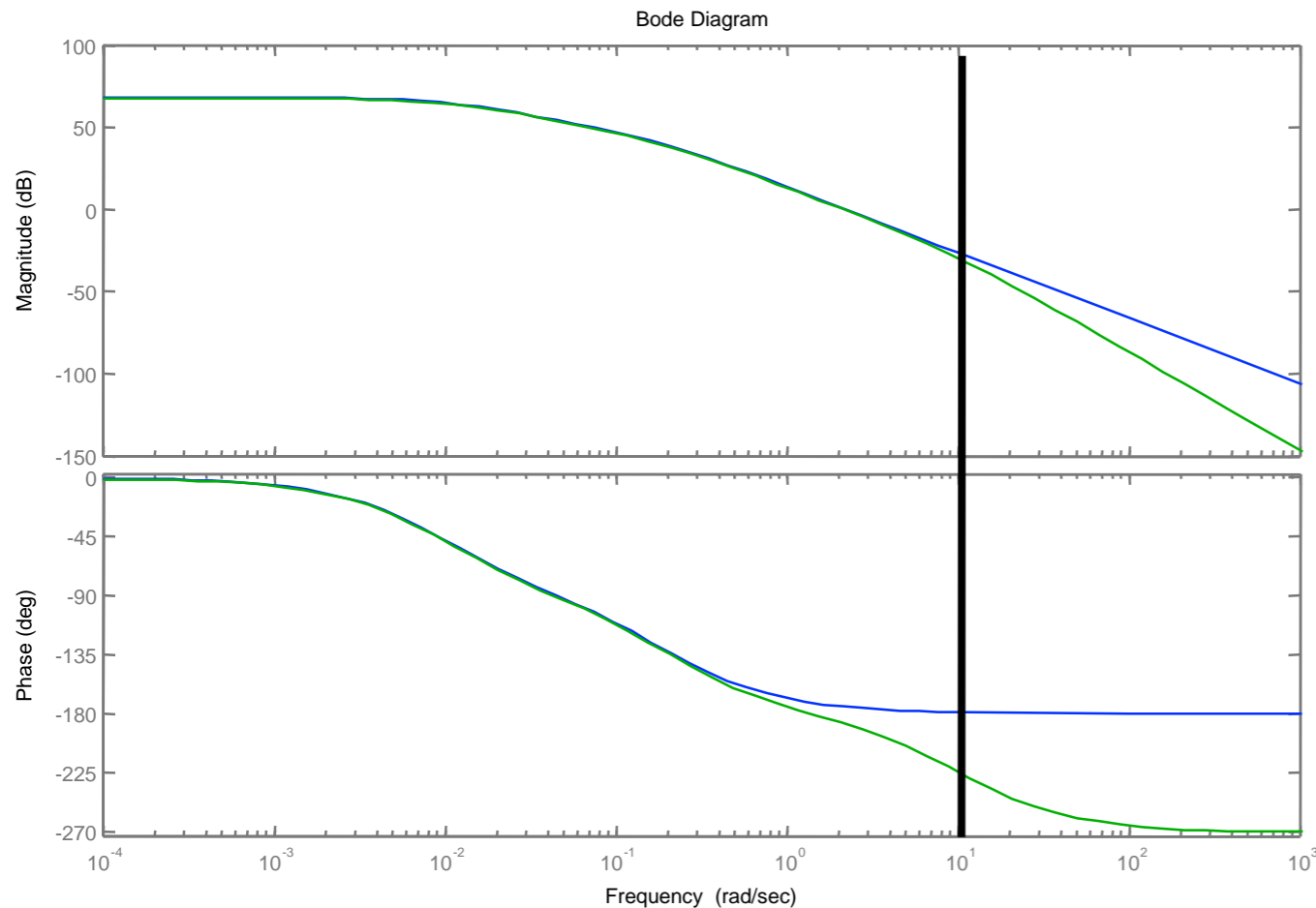
$$P(s) = \frac{1/m}{s + b/m} \times \frac{r}{s + a}$$

$$C(s) = K_p + \frac{K_i}{s + 0.01}$$

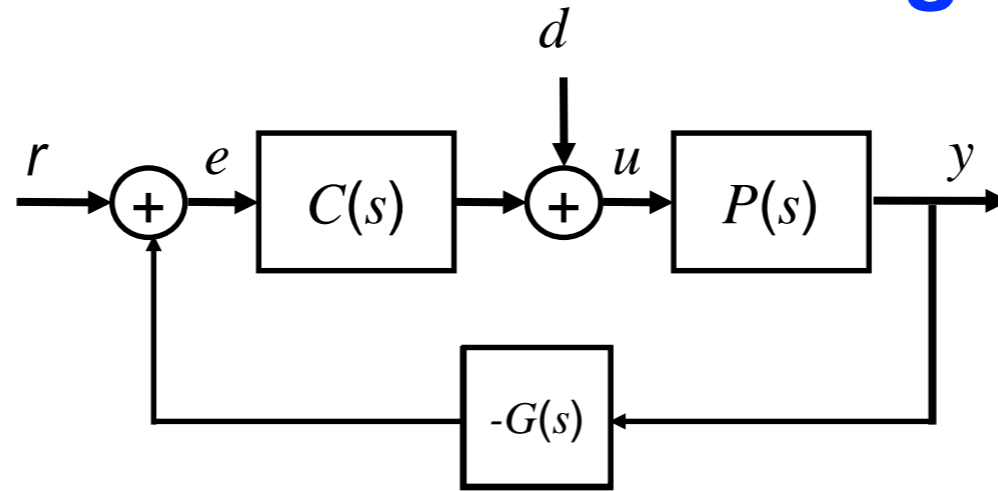
$$G(s) = \frac{10}{s + 10}$$

## Effect of additional sensor dynamics

- New speedometer has pole at  $s = 10$  (very fast); problems develop in the field
- What's the problem? A: insufficient phase margin in original design (not robust)



# Preview: control design



$$P(s) = \frac{1/m}{s + b/m} \times \frac{r}{s + a}$$

$$C(s) = \alpha \left( K_p + \frac{K_i}{s + 0.01} \right)$$

$$G(s) = \frac{10}{s + 10}$$

## Approach: Increase phase margin

- Increase phase margin by reducing gain  $\Rightarrow$  can accommodate new sensor dynamics
- Tradeoff: lower gain at low frequencies  $\Rightarrow$  less bandwidth, larger steady state error

